



10 INDUSTRIAL AVE,
SUITE 3
MAHWAH NJ 07430

PHONE: 201.684.0055
FAX: 201.684.0066

July 30, 2021

Members of the Siting Council
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

RE: Notice of Exempt Modification
50 Maple Street, Branford, CT 06405
Latitude: 41.2742440000
Longitude: -72.8136560000
T-Mobile Site#: CT11328F – Anchor

Dear Ms. Bachman:

T-Mobile currently maintains nine (9) antennas at the 96-foot level of the existing 100-foot smokestack at 50 Maple Street, CT. The 100-foot smokestack and property are owned by Marine Systems Incorporated. T-Mobile now intends to replace six (6) existing antennas with six (6) new 1900/2100/2500 MHz antennas. The new antennas will support 5G services and will be installed at the same 96-foot level of the tower.

Planned Modifications:

Tower:

Remove

(3) TMA

Remove and Replace:

(3) AIR 21 for (3) RFS APX16DWV-16DWV-S-E-A20 1900/2100 MHz antennas

(3) AIR 21 for (3) Ericsson AIR 6449 2500 MHz antennas

Install New:

(3) Radio 4460 B25+B66

(3) 1-5/8" Hybrid

Existing to Remain:

(3) APXVAALL24_43-U-NA20

(3) Radio 4449 B75+B85

(3) 1-5/8" Hybrid

(6) 1-5/8" coax

The original approval of this facility was by the Town of Branford Planning and Zoning Commission. The Commission approved the facility on January 7, 2010. A copy of this approval is enclosed. T-Mobile was subsequently approved for tower-sharing by the Connecticut Siting Council on March 3, 2017.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to First Selectman -James Cosgrove, Elected Official, and Harry Smith, Town Planner, as well as the owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

Kyle Richers

Transcend Wireless

Cell: 908-447-4716

Email: krichers@transcendwireless.com

Attachments

cc: James Cosgrove – First Selectman – Town of Branford
Harry Smith – Town Planner – Town of Branford
Marine Systems Inc – Owner

Kyle Richers

From: UPS <pkginfo@ups.com>
Sent: Wednesday, August 4, 2021 10:09 AM
To: KRICHERS@TRANSCENDWIRELESS.COM
Subject: UPS Delivery Notification, Tracking Number 1ZV257424297944826



Hello, your package has been delivered.

Delivery Date: Wednesday, 08/04/2021

Delivery Time: 10:07 AM

Left At: RECEPTION

Signed by: TRISTA M

TRANSCEND WIRELESS

Tracking Number: [1ZV257424297944826](#)

Ship To: TOWN OF BRANFORD
1019 MAIN STREET
BRANFORD, CT 06405
US

Number of Packages: 1

UPS Service: UPS Ground

Package Weight: 1.0 LBS

Reference Number: CT11328F CSC EO



[Download the UPS mobile app](#)

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All trademarks, trade names, or service marks that appear in connection with UPS's services are the property of their respective owners.

Please do not reply directly to this email. UPS will not receive any reply message.

Kyle Richers

From: UPS <pkginfo@ups.com>
Sent: Wednesday, August 4, 2021 10:09 AM
To: KRICHERS@TRANSCENDWIRELESS.COM
Subject: UPS Delivery Notification, Tracking Number 1ZV257424297614834



Hello, your package has been delivered.

Delivery Date: Wednesday, 08/04/2021

Delivery Time: 10:07 AM

Left At: RECEPTION

Signed by: TRISTA M

TRANSCEND WIRELESS

Tracking Number: [1ZV257424297614834](#)

Ship To: TOWN OF BRANFORD
1019 MAIN STREET
BRANFORD, CT 06405
US

Number of Packages: 1

UPS Service: UPS Ground

Package Weight: 1.0 LBS

Reference Number: CT11328F UPS 3



[Download the UPS mobile app](#)

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Please do not reply directly to this email. UPS will not receive any reply message.

Kyle Richers

From: UPS <auto-notify@ups.com>
Sent: Tuesday, August 3, 2021 10:02 PM
To: krichers@transcendwireless.com
Subject: UPS Exception Notification, Tracking Number 1ZV257424294431582



The status of your package has changed.

Exception Reason: Due to operating conditions, your delivery may be delayed.

Exception Resolution: The package will be forwarded to a UPS facility in the destination city.

At the request of TRANSCEND WIRELESS, this notice alerts you that the status of the shipment listed below has changed.

Signature Required: A signature is required for package delivery

Shipment Details

Tracking Number: [1ZV257424294431582](#)
Ship To: Marine Systems Inc.
50 Maple Street
BRANFORD, CT 06405
US
UPS Service: UPS GROUND
Package Weight: 1.0 LBS
Reference Number 1: CT11328F CSC 1



50 MAPLE ST

Location 50 MAPLE ST

Mblu D08/000 012/ 00003/ /

Acct# 000592

Owner MARINE SYSTEMS
INCORPORATED

Assessment \$964,500

Appraisal \$1,378,100

PID 801

Building Count 2

Current Value

Appraisal			
Valuation Year	Improvements	Land	Total
2019	\$412,300	\$965,800	\$1,378,100

Assessment			
Valuation Year	Improvements	Land	Total
2019	\$288,400	\$676,100	\$964,500

Owner of Record

Owner MARINE SYSTEMS INCORPORATED
Co-Owner
Address PO BOX 447
BRANFORD, CT 06405

Sale Price \$0
Certificate
Book & Page 0555/1008
Sale Date 09/07/1993

Ownership History

Ownership History				
Owner	Sale Price	Certificate	Book & Page	Sale Date
MARINE SYSTEMS INCORPORATED	\$0		0555/1008	09/07/1993

Building Information

Building 1 : Section 1

Year Built: 1900
Living Area: 82,765
Replacement Cost: \$3,139,276
Building Percent Good: 3
Replacement Cost
Less Depreciation: \$94,200

Building Attributes

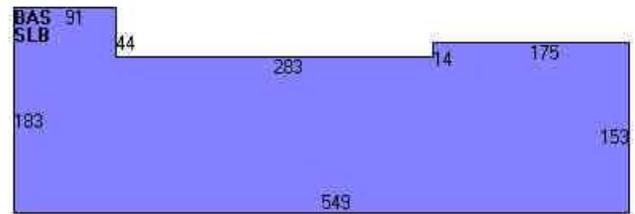
Field	Description
STYLE	Warehouse
MODEL	Ind/Comm
Grade	C
Stories:	1
Occupancy	3
Exterior Wall 1	Brick
Exterior Wall 2	Concr/Cinder
Roof Structure	Flat
Roof Cover	T&G/Rubber
Interior Wall 1	Minim/Masonry
Interior Wall 2	
Interior Floor 1	Concr-Finished
Interior Floor 2	
Heating Fuel	None/Coal/Wd
Heating Type	None
AC Type	None
Bldg Use	BOATYARD MDL96
Total Rooms	
Total Bedrms	00
Total Baths	0
1st Floor Use:	3841
Heat/AC	NONE
Frame Type	MASONRY
Baths/Plumbing	LIGHT
Ceiling/Wall	NONE
Rooms/Prtns	AVERAGE
Wall Height	22
% Comn Wall	

Building Photo



(<http://images.vgsi.com/photos/BranfordCTPhotos/\A00\01\54\82.jpg>)

Building Layout



(http://images.vgsi.com/photos/BranfordCTPhotos//Sketches/801_801.jpg)

Building Sub-Areas (sq ft)			Legend
Code	Description	Gross Area	Living Area
BAS	First Floor	82,765	82,765
SLB	Slab	82,765	0
		165,530	82,765

Building 2 : Section 1

Year Built: 1920
Living Area: 2,304
Replacement Cost: \$277,502
Building Percent Good: 30
Replacement Cost Less Depreciation: \$83,300

Building Attributes : Bldg 2 of 2	
Field	Description
STYLE	Restaurant
MODEL	Comm/Ind
Grade	C

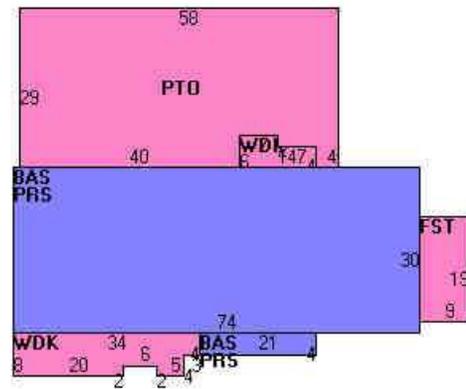
Stories:	1
Occupancy	1
Exterior Wall 1	Wood Shingle
Exterior Wall 2	
Roof Structure	Gable/Hip
Roof Cover	Asphalt
Interior Wall 1	Drywall
Interior Wall 2	
Interior Floor 1	Hardwood
Interior Floor 2	Ceram Clay Til
Heating Fuel	Gas
Heating Type	Forced Air-Duc
AC Type	Central
Bldg Use	REST/CLUBS MDL94
Total Rooms	
Total Bedrms	00
Total Baths	0
1st Floor Use:	3840
Heat/AC	HEAT/AC SPLIT
Frame Type	WOOD FRAME
Baths/Plumbing	AVERAGE
Ceiling/Wall	CEIL & WALLS
Rooms/Prtns	AVERAGE
Wall Height	8
% Comn Wall	

Building Photo



(<http://images.vgsi.com/photos/BranfordCTPhotos/\A00\02\16\71.jpg>)

Building Layout



(http://images.vgsi.com/photos/BranfordCTPhotos//Sketches/801_14082.jp)

Building Sub-Areas (sq ft)			Legend
Code	Description	Gross Area	Living Area
BAS	First Floor	2,304	2,304
FST	Utility, Finished	171	0
PRS	Pier Fndtn	2,304	0
PTO	Patio	1,612	0
WDK	Deck, Wood	318	0
		6,709	2,304

Extra Features

Extra Features				Legend
Code	Description	Size	Value	Bldg #
MEZ1	MEZZANINE-UNF	784 S.F.	\$200	1
GIR3	GIRDERS 19"-24	80 L.F.	\$200	1
HT2	ELECTRIC	1248 S.F.	\$200	1

HT3	FORCED AIR	840 S.F.	\$200	1
A/C	AIR CONDITION	0 S.F.	\$0	1

Land

Land Use

Use Code 3150
Description BOATYARD MDL96
Zone IG-1
Neighborhood 350
Alt Land Appr No
Category

Land Line Valuation

Size (Acres) 4.59
Frontage
Depth
Assessed Value \$676,100
Appraised Value \$965,800

Outbuildings

Outbuildings						Legend
Code	Description	Sub Code	Sub Description	Size	Value	Bldg #
PAV1	PAVING-ASPHALT			36978 S.F.	\$18,300	1
SHD5	SHED COM WOOD			168 S.F.	\$1,400	2
PAV2	PAVING-CONC			3204 S.F.	\$3,200	1
LT1	LIGHTS-IN W/PL			1 UNITS	\$200	1
LT1	LIGHTS-IN W/PL			1 UNITS	\$200	1
LT2	W/DOUBLE LIGHT			2 UNITS	\$700	1
FN3	FENCE-6' CHAIN			510 L.F.	\$1,500	1
WDK	WOOD DECK			230 S.F.	\$700	1
DCK3	FLOATING			4507 S.F.	\$114,900	1
DCK3	FLOATING			2804 S.F.	\$71,500	1
STK1	CHIMNEY STK BR			100 UNITS	\$20,000	1
SHD5	SHED COM WOOD			160 S.F.	\$1,400	1

Valuation History

Appraisal			
Valuation Year	Improvements	Land	Total
2020	\$412,300	\$965,800	\$1,378,100
2019	\$412,300	\$965,800	\$1,378,100
2018	\$401,900	\$937,400	\$1,339,300

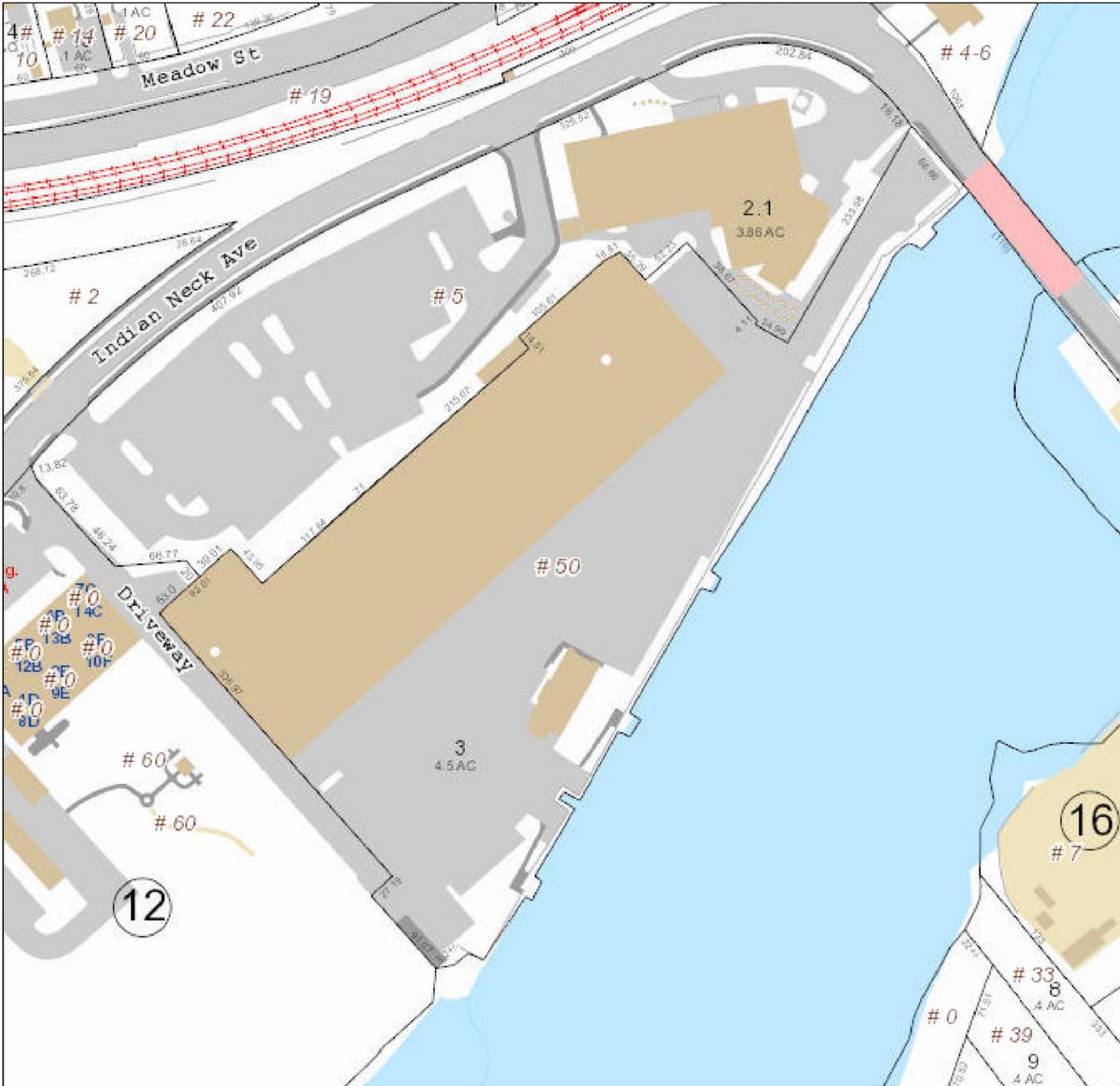
Assessment			
Valuation Year	Improvements	Land	Total
2020	\$288,400	\$676,100	\$964,500
2019	\$288,400	\$676,100	\$964,500
2018	\$281,300	\$656,200	\$937,500

Town of Branford

Geographic Information System (GIS)

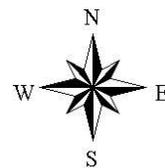


Date Printed: 4/16/2021



MAP DISCLAIMER - NOTICE OF LIABILITY

This map is for assessment purposes only. It is not for legal description or conveyances. All information is subject to verification by any user. The Town of Branford and its mapping contractors assume no legal responsibility for the information contained herein.



PLANNING AND ZONING COMMISSION
TOWN OF BRANFORD TOWN HALL DRIVE P.O. BOX 150
Branford, Connecticut 06405
Telephone: (203) 488-1255 Fax: (203) 315-2188

NOTICE OF DECISION

January 11, 2010

Clearwire by Maxton Technology
Attention: Thomas F. Flynn III
1296 Blue Hills Avenue
Bloomfield, Connecticut 06002

SUBJECT: Site Plan

APPLICATION: #09-12.4 ADDRESS: 50 Maple Street

APPLICANT: Clearwire Wireless LLC d/b/a Clearwire

OWNER OF RECORD: Marine Systems, Inc.

Dear Sir:

At a meeting of the Branford Planning & Zoning Commission held on Thursday, January 7, 2010 the Commission voted to:

Approve your above subject application.

Very truly yours,



Shirley Rasmussen
Town Planner

NOTE: Site Plan shall become null and void in the event the applicant fails to obtain a building permit within one (1) year of date of approval.
(Per Section 31.7 of the Branford Zoning Regulations)

PLANNING AND ZONING COMMISSION
TOWN OF BRANFORD TOWN HALL DRIVE P.O. BOX 150
Branford, Connecticut 06405
Telephone: (203) 488-1255 Fax: (203) 315-2188

NOTICE OF DECISION

January 11, 2010

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Bloomfield, Connecticut 06002

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APPLICANT: Clearwire Wireless LLC d/b/a Clearwire

OWNER OF RECORD: Marine Systems, Inc.

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Very truly yours,



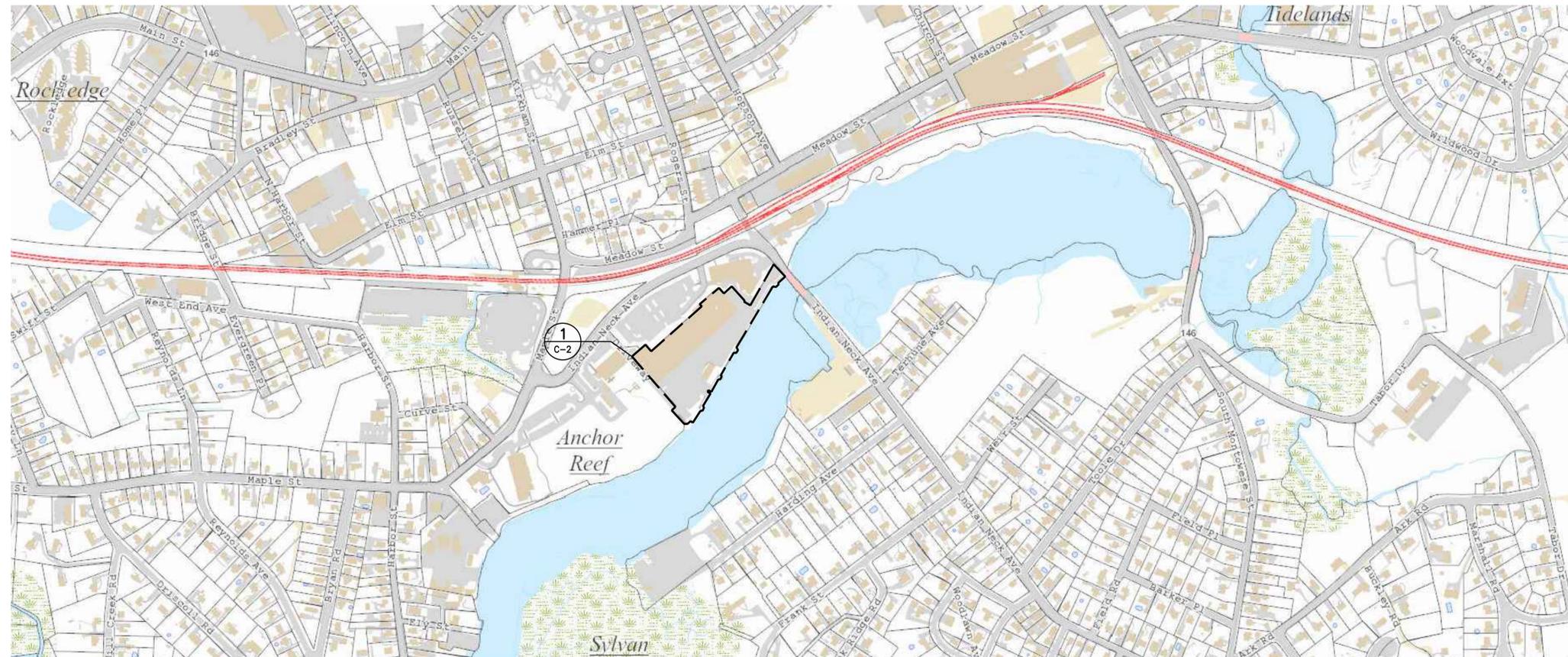
Shirley Rasmussen
Town Planner

NOTE: Site Plan shall become null and void in the event the applicant fails to obtain a building permit within one (1) year of date of approval.
(Per Section 31.7 of the Branford Zoning Regulations)

NOTE:
ALL HCS LENGTHS TO BE MEASURED AND
VERIFIED IN FIELD BEFORE ORDERING

ANTENNA SCHEDULE

SECTOR	EXISTING/PROPOSED	ANTENNA	SIZE (INCHES) (L x W x D)	ANTENNA Q HEIGHT	AZIMUTH	(E/P) RRU (QTY)	(E/P) TMA (QTY)	(QTY) EXISTING COAX
A1	PROPOSED	ERICSSON (AIR6449 B41)	33.1 x 20.6 x 8.6	96'	60°			(1) 6x24 HYBRID CABLE
A2	EXISTING	RFS (APXVAALL24_43-U-NA20)	95.9 x 24 x 8.5	96'	60°	(E) RADIO 4449 B71+B85 (1)		
A3	PROPOSED	RFS (APX16DWV-16DWV-S-E-A20)	55.9 x 13 x 3.15	96'	60°	(P) RADIO 4460 B25+B66 (1)		
B1	PROPOSED	ERICSSON (AIR6449 B41)	33.1 x 20.6 x 8.6	96'	180°			(1) 6x24 HYBRID CABLE
B2	EXISTING	RFS-APXVAALL24_43-U-NA20	95.9 x 24 x 8.5	96'	180°	(E) RADIO 4449 B71+B85 (1)		
B3	PROPOSED	RFS (APX16DWV-16DWV-S-E-A20)	55.9 x 13 x 3.15	96'	180°	(P) RADIO 4460 B25+B66 (1)		
C1	PROPOSED	ERICSSON (AIR6449 B41)	33.1 x 20.6 x 8.6	96'	300°			(1) 6x24 HYBRID CABLE
C2	EXISTING	RFS-APXVAALL24_43-U-NA20	95.9 x 24 x 8.5	96'	300°	(E) RADIO 4449 B71+B85 (1)		
C3	PROPOSED	RFS (APX16DWV-16DWV-S-E-A20)	55.9 x 13 x 3.15	96'	300°	(P) RADIO 4460 B25+B66 (1)		



1 SITE LOCATION PLAN
C-1 SCALE: NOT TO SCALE



PROFESSIONAL ENGINEER SEAL



T-Mobile
T-Mobile
T-Mobile

CENTER engineering
Centered on Solutions
(203) 488-0580
(203) 488-8587 Fax
65-2 North Branford Road
Branford, CT 06405
www.CenterEng.com

T-MOBILE NORTHEAST LLC
MARINE SYS SMOKE STACK
SITE ID: CT11328F
50 MAPLE STREET,
BRANFORD, CT 06405

DATE: 06/30/21
SCALE: AS NOTED
JOB NO. 21022.22

SITE LOCATION
PLAN

C-1

REV. DATE 07/23/21
DRAWN BY: TJR
CHECKED BY: BSP
CONSTRUCTION DRAWINGS - ISSUED FOR CONSTRUCTION

STRUCTURAL COMPLIANCE

ANTENNA MOUNTS

A STRUCTURAL ANALYSIS OF THE ANTENNA MOUNTS WAS PERFORMED FOR THE PROPOSED EQUIPMENT INSTALLATION AND THEY WERE FOUND TO BE STRUCTURALLY SUFFICIENT TO ACCOMMODATE THE PROPOSED LOADING..

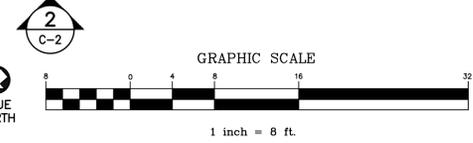
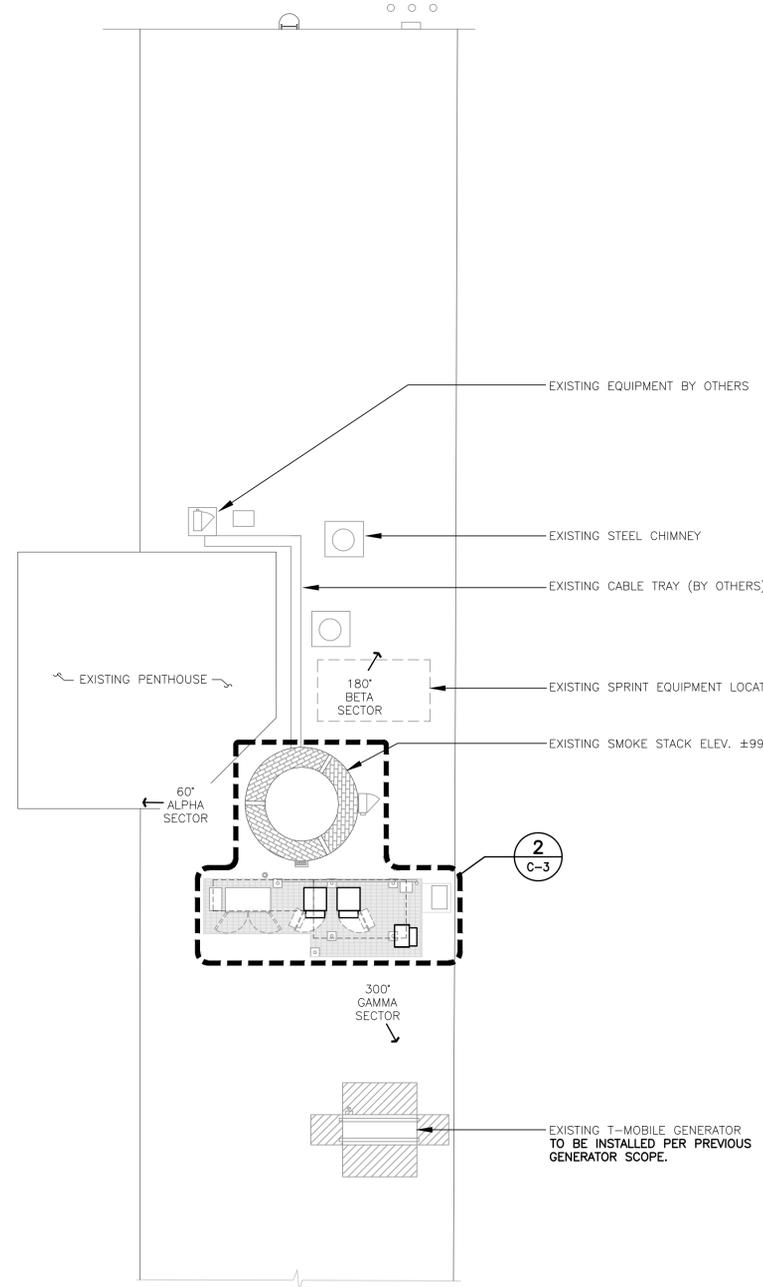
REFER TO THE ANTENNA MOUNT ANALYSIS REPORT PREPARED BY CENTEK ENGINEERING (PROJECT # 21022.22) DATED 07/06/21 FOR ADDITIONAL INFORMATION AND REQUIREMENTS.

MASONRY SMOKESTACK AND HOST BUILDING

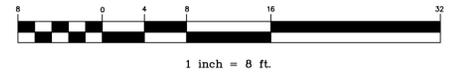
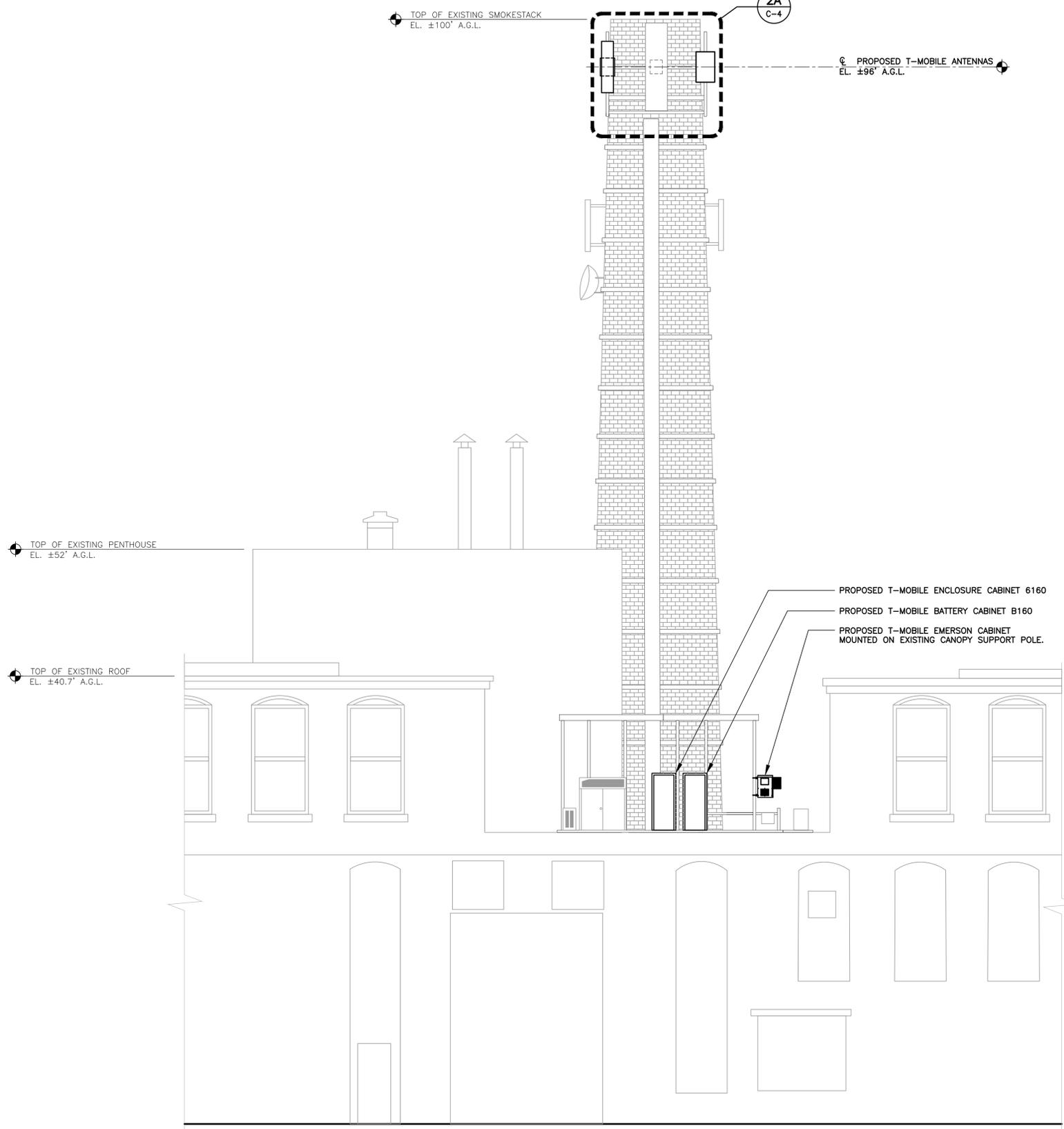
A STRUCTURAL ANALYSIS OF THE MASONRY SMOKESTACK AND HOST BUILDING WAS PERFORMED FOR THE PROPOSED EQUIPMENT INSTALLATION AND THEY WERE FOUND TO BE STRUCTURALLY SUFFICIENT TO ACCOMMODATE THE PROPOSED LOADING.

REFER TO THE STRUCTURAL ANALYSIS REPORT PREPARED BY CENTEK ENGINEERING (PROJECT # 21022.22) DATED 07/06/21 FOR ADDITIONAL INFORMATION AND REQUIREMENTS.

NOTE: NO EQUIPMENT SHALL BE INSTALLED ON THE HOSTING STRUCTURE WITHOUT A PASSING STRUCTURAL ANALYSIS REPORT AND CONTRACTOR PRIOR CONFIRMATION THAT ANY AND ALL REQUISITE MODIFICATIONS HAVE BEEN COMPLETED.

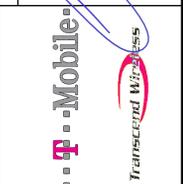


1 PARTIAL COMPOUND PLAN
SCALE: 1" = 8'
TRUE NORTH



2 NORTH ELEVATION
SCALE: 1" = 8'

REV.	DATE	BY	CHK'D BY	DESCRIPTION
0	07/23/21	BSF	TJR	CONSTRUCTION DRAWINGS - ISSUED FOR CONSTRUCTION



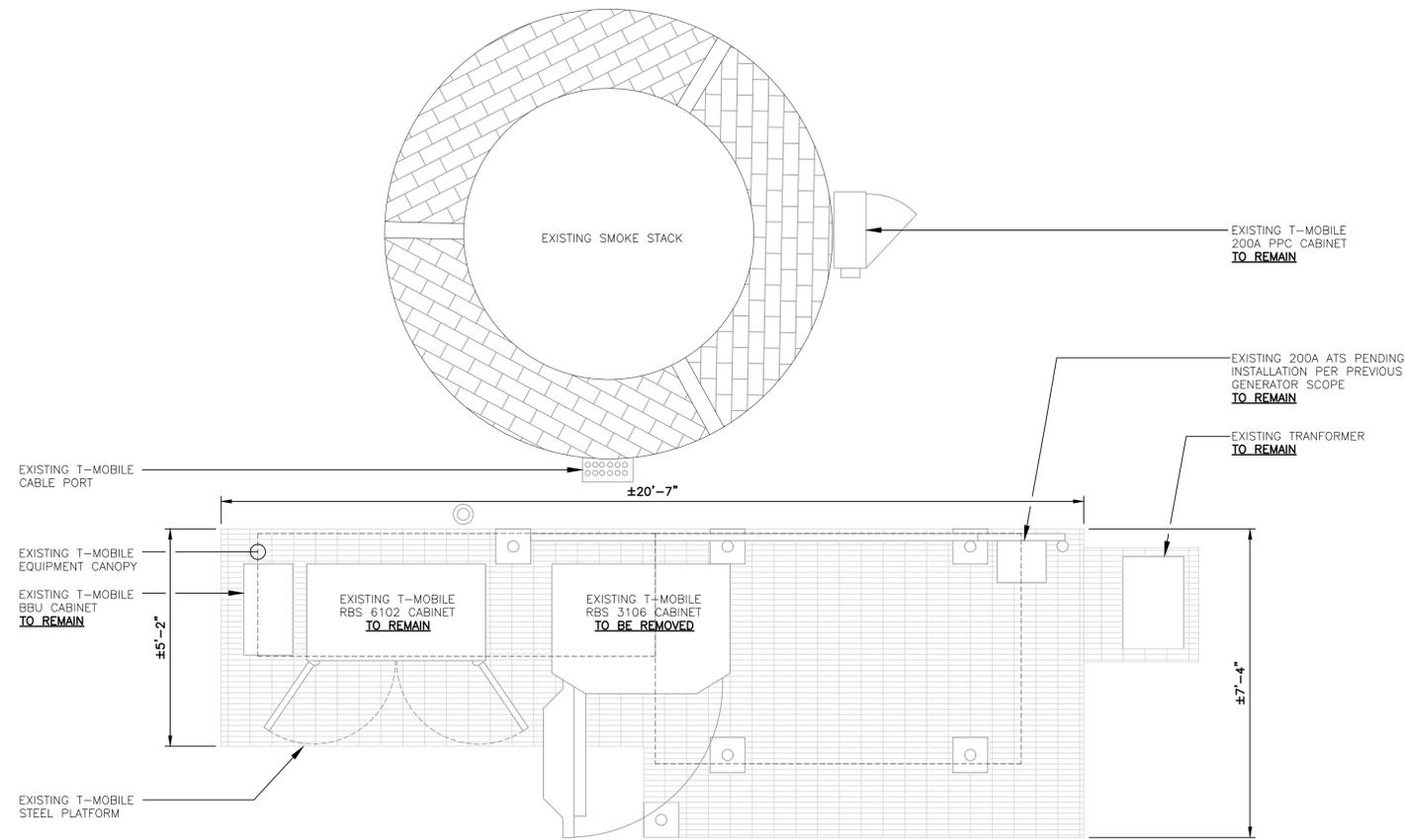
CEN TEK engineering
Centered on Solutions
(203) 488-0380
(203) 488-8587 Fax
63-2 North Branford Road
Branford, CT 06405
www.CentekEng.com

T-MOBILE NORTHEAST LLC
MARINE SYS SMOKE STACK
SITE ID: CT11328F
50 MAPLE STREET,
BRANFORD, CT 06405

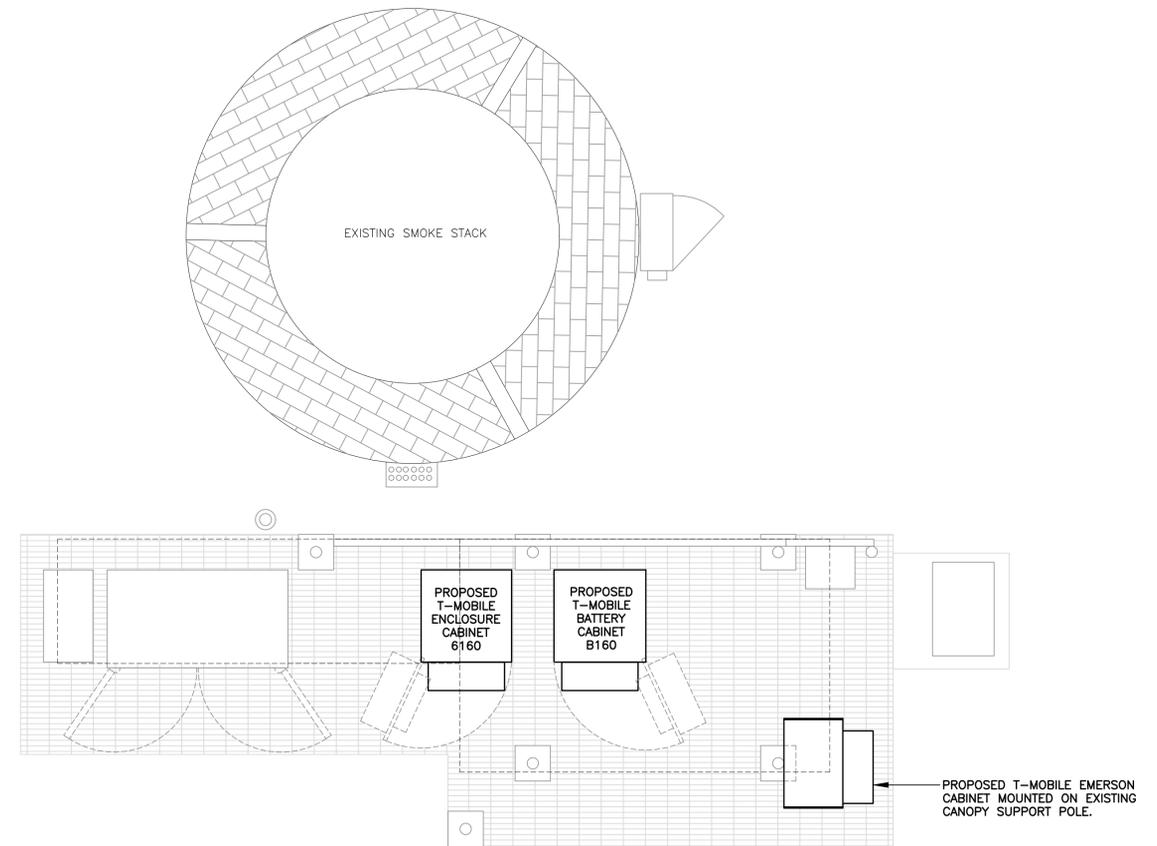
DATE: 06/30/21
SCALE: AS NOTED
JOB NO. 21022.22

PARTIAL COMPOUND PLAN AND ELEVATION

C-2
Sheet No. 4 of 11



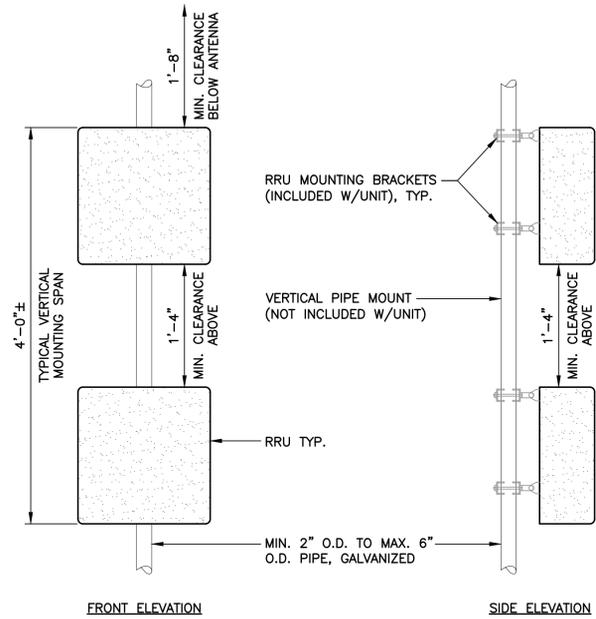
1 EXISTING EQUIPMENT PLAN
 C-3 SCALE: 1/2" = 1' TRUE NORTH



2 PROPOSED EQUIPMENT PLAN
 C-3 SCALE: 1/2" = 1' TRUE NORTH

(203) 488-0580 (203) 488-8587 Fax 63-2 North Branford Road Branford, CT 06405 www.CentexEng.com	
T-MOBILE NORTHEAST LLC MARINE SYS SMOKE STACK SITE ID: CT11328F 50 MAPLE STREET, BRANFORD, CT 06405	
DATE:	06/30/21
SCALE:	AS NOTED
JOB NO.	21022.22
EQUIPMENT PLANS	
<h1>C-3</h1>	
Sheet No. 5 of 11	

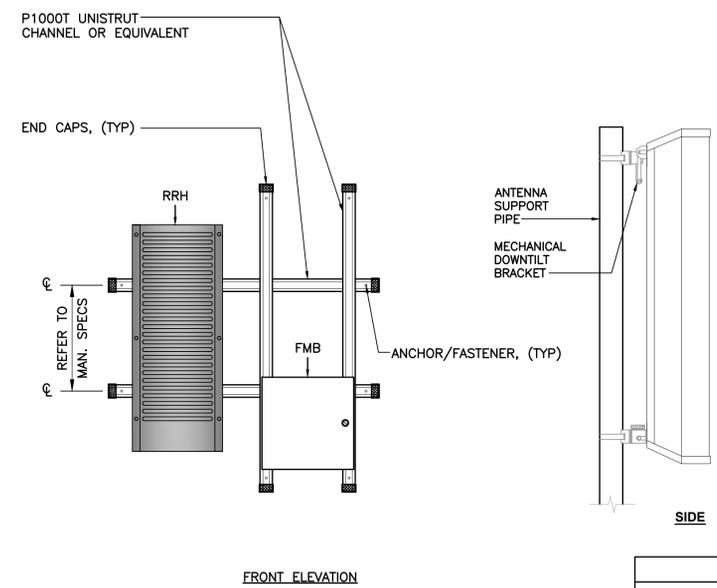
REV.	DATE	BY	CHK'D BY	DESCRIPTION
0	07/23/21	BSF	TJR	CONSTRUCTION DRAWINGS - ISSUED FOR CONSTRUCTION



NOTES: (PIPE MOUNTING)

- T-MOBILE SHALL SUPPLY RRU, AND RRU POLE-MOUNTING BRACKET. CONTRACTOR SHALL SUPPLY POLE/PIPE AND INSTALL ALL MOUNTING HARDWARE INCLUDING ERICSSON RRU POLE-MOUNTING BRACKET.
- NO PAINTING OF THE RRU OR SOLAR SHIELD IS ALLOWED.

1 TYPICAL RRU MOUNTING DETAILS
C-5 SCALE: NOT TO SCALE



NOTES: (UNISTRUT MOUNTING)

- INSTALL A MINIMUM OF (2) ANCHORS PER UNISTRUT ($\pm 16^\circ/c$ MIN).
- MOUNT RRU TO UNISTRUT WITH 3/8" UNISTRUT BOLTING HARDWARE AND SPRING NUTS. TYPICAL FOUR PER BRACKET.
- NO PAINTING OF THE RRU OR SOLAR SHIELD IS ALLOWED.

2 PROPOSED ANTENNA DETAIL
C-5 SCALE: NOT TO SCALE

ALPHA/BETA/GAMMA ANTENNA		
EQUIPMENT	DIMENSIONS	WEIGHT
MAKE: ERICSSON MODEL: AIR6449 B41	33.1"L x 20.6"W x 8.6"D	±104 LBS.
MAKE: RFS MODEL: APX16DWV-16DWV-S-E-A20	55.9"L x 13"W x 3.15"D	±40.7 LBS.

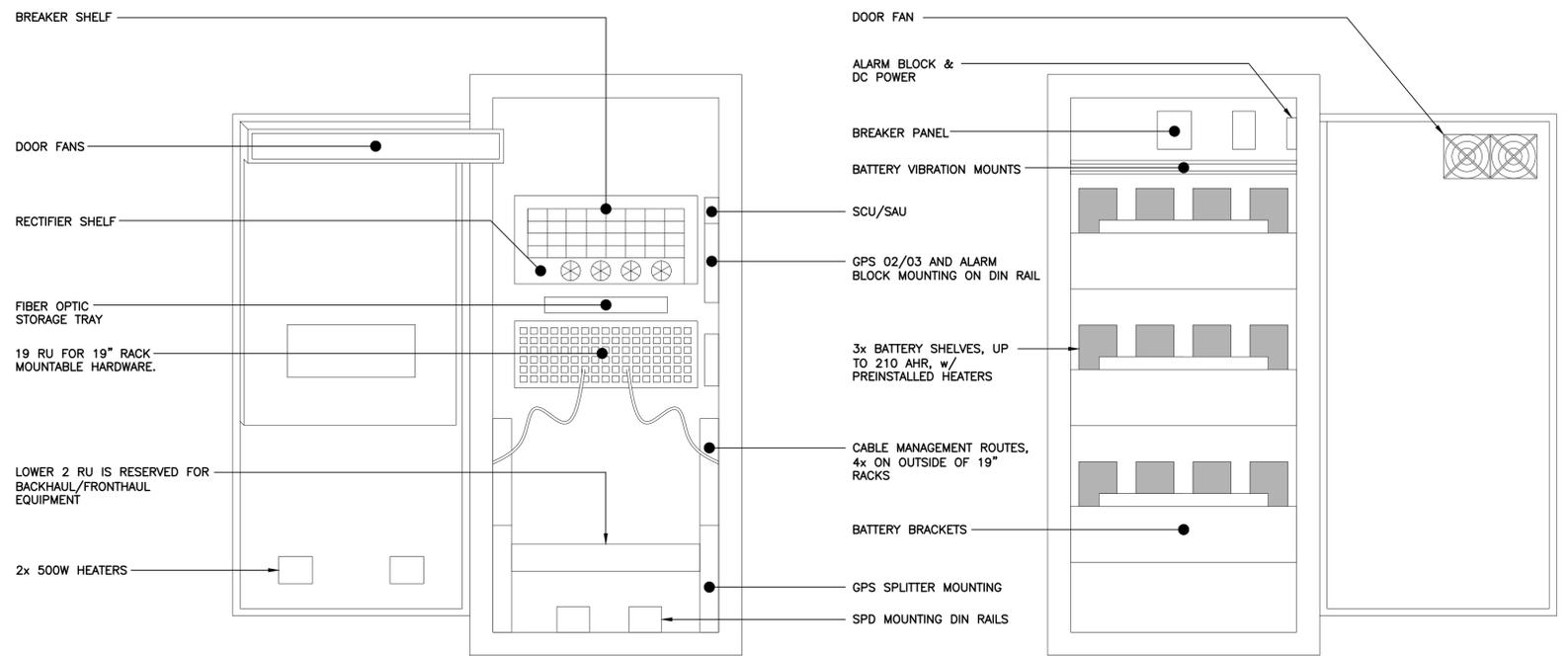
NOTES:
1. CONTRACTOR TO COORDINATE FINAL EQUIPMENT MODEL SELECTION WITH T-MOBILE CONSTRUCTION MANAGER PRIOR TO ORDERING.



RRU (REMOTE RADIO UNIT)			
EQUIPMENT	DIMENSIONS	WEIGHT	CLEARANCES
MAKE: ERICSSON MODEL: RADIO 4460 B25+B66	19.6"L x 15.7"W x 12.1"D	±109 LBS.	BEHIND ANT.: 8" MIN. BELOW ANT.: 20" MIN. BELOW RRU: 16" MIN.

NOTES:
1. CONTRACTOR TO COORDINATE FINAL EQUIPMENT MODEL SELECTION WITH T-MOBILE CONSTRUCTION MANAGER PRIOR TO ORDERING.

3 PROPOSED RRU DETAIL
C-5 SCALE: NOT TO SCALE

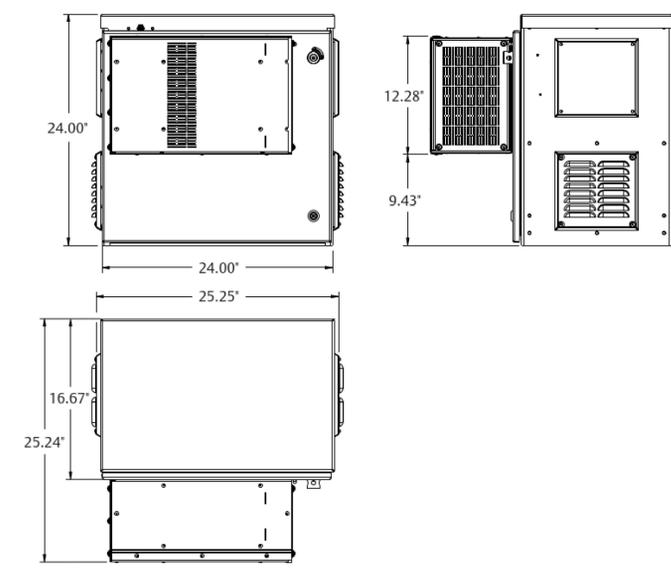


EQUIPMENT CABINET		
EQUIPMENT	DIMENSIONS	WEIGHT
MAKE: ERICSSON MODEL: ENCLOSURE 6160 CABINET	62.0"H x 26.0"W x 26.0"D	±1200 LBS

4 ENCLOSURE 6160 CABINET DETAIL
C-5 SCALE: NOT TO SCALE

EQUIPMENT CABINET		
EQUIPMENT	DIMENSIONS	WEIGHT
MAKE: ERICSSON MODEL: BATTERY B160 CABINET	62.0"H x 26.0"W x 26.0"D	±1883 LBS

5 BATTERY B160 CABINET DETAIL
C-5 SCALE: NOT TO SCALE



EMERSON CABINET		
EQUIPMENT	DIMENSIONS	WEIGHT
MAKE: EMERSON MODEL: COMPACT 2416	24"L x 24"W x 16"D	±64 LBS.

NOTES:
1. CONTRACTOR TO COORDINATE FINAL EQUIPMENT MODEL SELECTION WITH T-MOBILE CONSTRUCTION MANAGER PRIOR TO ORDERING.

6 PROPOSED EMERSON CABINET DETAIL
C-5 SCALE: NOT TO SCALE

PROFESSIONAL ENGINEER SEAL

T-Mobile

CENTER engineering
Centered on Solutions
(203) 489-0380
(203) 488-8587 Fax
65-2 North Branford Road
Branford, CT 06405
www.CenterEng.com

T-MOBILE NORTHEAST LLC
MARINE SYS SMOKE STACK
SITE ID: CT11328F
50 MAPLE STREET,
BRANFORD, CT 06405

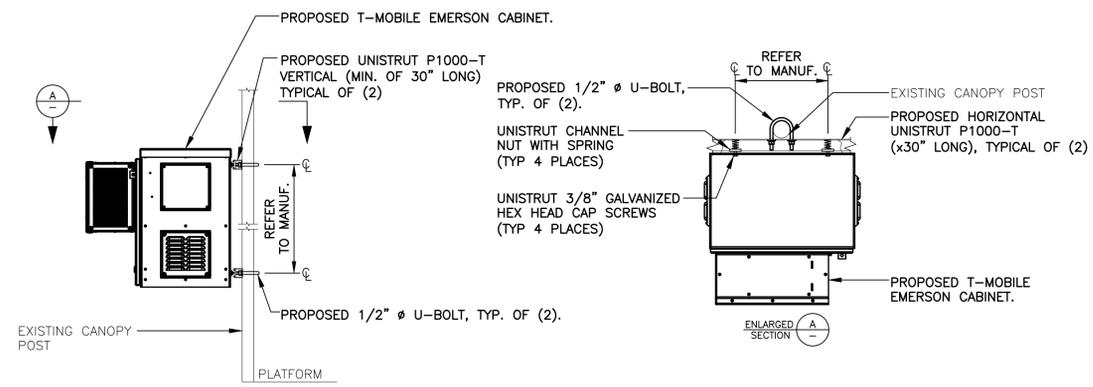
DATE: 06/30/21
SCALE: AS NOTED
JOB NO. 21022.22

TYPICAL EQUIPMENT DETAILS

C-5

Sheet No. 7 of 11

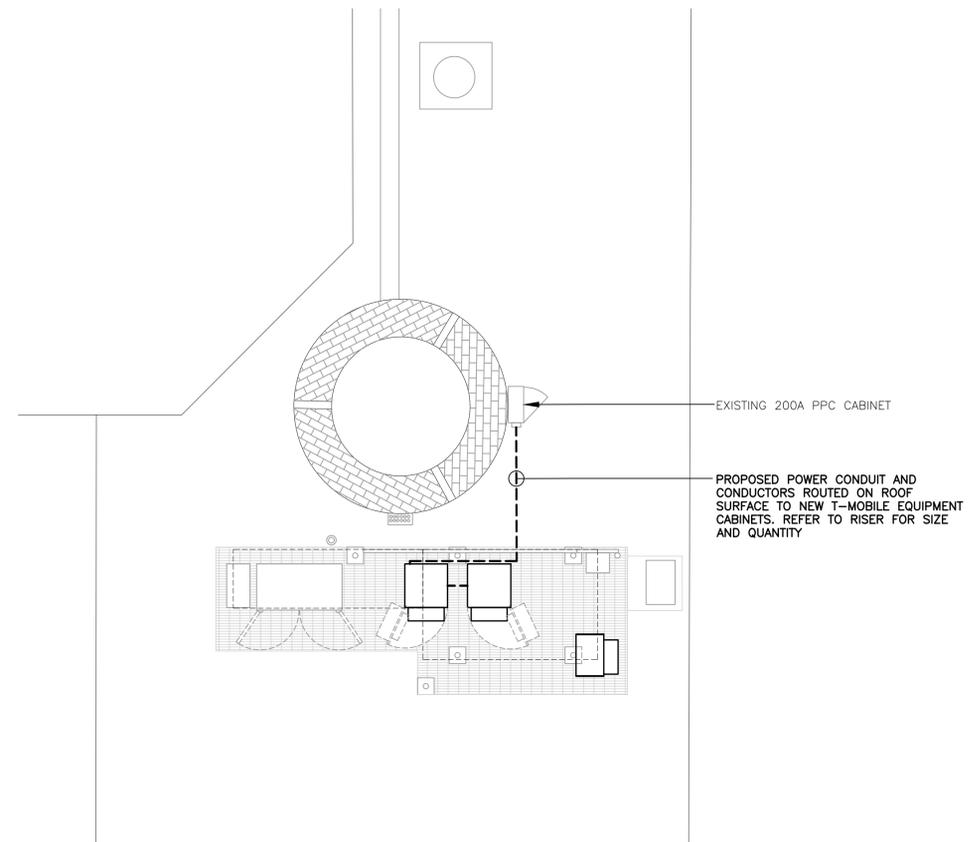
CONSTRUCTION DRAWINGS - ISSUED FOR CONSTRUCTION
REV. DATE DRAWN BY/CHK'D BY DESCRIPTION



1
S-1 TYPICAL APPURTENANCE MOUNTING DETAIL
SCALE: NOT TO SCALE

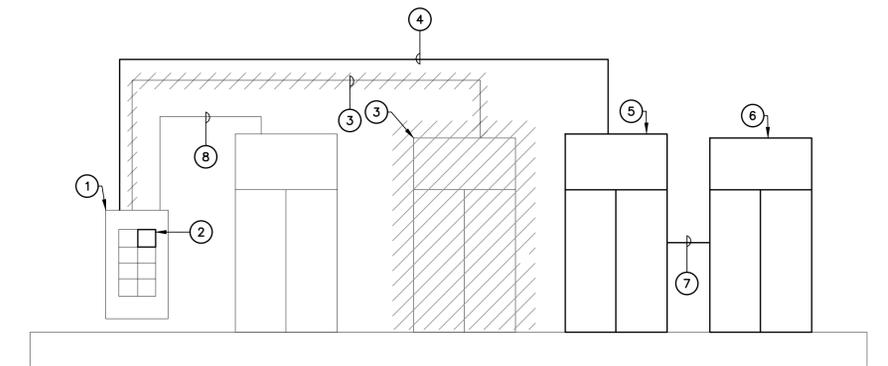
<p>(203) 488-0580 (203) 488-8587 Fax 65-2 North Branford Road Branford, CT 06405 www.CentekEng.com</p>	
<p>T-MOBILE NORTHEAST LLC MARINE SYS SMOKE STACK SITE ID: CT11328F 50 MAPLE STREET, BRANFORD, CT 06405</p>	
DATE:	06/30/21
SCALE:	AS NOTED
JOB NO.	21022.22
EQUIPMENT MOUNTING DETAILS	
S-1	
Sheet No. 8 of 11	

REV.	DATE	BY	CHK'D BY	DESCRIPTION
0	07/23/21	BSF	TJR	CONSTRUCTION DRAWINGS - ISSUED FOR CONSTRUCTION



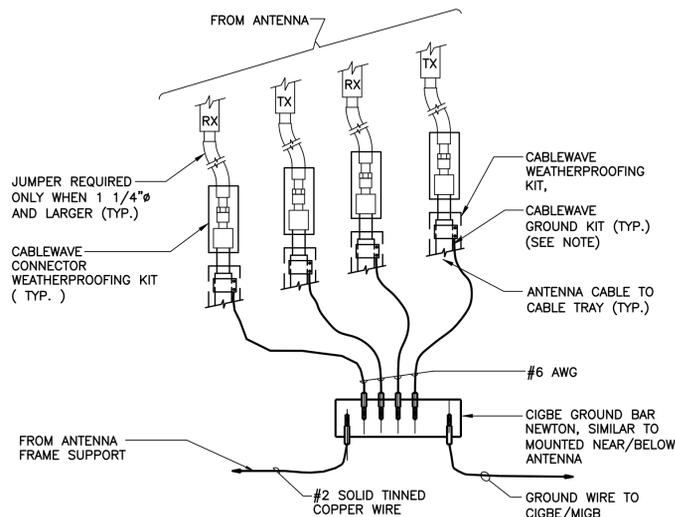
1 ELECTRICAL CONDUIT ROUTING PLAN
E-1 SCALE: NOT TO SCALE

- RISER DIAGRAM NOTES**
- ① EXISTING 200A, PPC CABINET TO REMAIN.
 - ② NEW 150A/2P CIRCUIT BREAKER TO SERVE NEW EQUIPMENT
 - ③ EXISTING CABINETS AND ASSOCIATED CONDUITS AND CONDUCTORS TO BE REMOVED.
 - ④ (3) 1/0 AWG, (1) #6 AWG GROUND, 2" CONDUIT.
 - ⑤ NEW T-MOBILE EQUIPMENT CABINET
 - ⑥ NEW T-MOBILE BATTERY CABINET
 - ⑦ DC CONDUIT AND CONDUCTORS FOR BATTERY CABINET CONNECTION PER MANUFACTURERS SPECIFICATIONS.
 - ⑧ EXISTING CABINET AND ASSOCIATED CONDUIT AND CONDUCTORS TO REMAIN



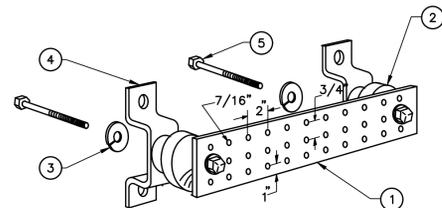
2 ELECTRICAL POWER RISER DIAGRAM
E-1 SCALE: NOT TO SCALE

			T-MOBILE NORTHEAST LLC MARINE SYS SMOKE STACK SITE ID: CT11328F 50 MAPLE STREET, BRANFORD, CT 06405					
PROFESSIONAL ENGINEER SEAL STATE OF CONNECTICUT T. J. RAY LICENSE NO. 14233-ES-5	T-Mobile T-Mobile 14233-ES-5	CENTEK engineering Centered on Solutions (203) 488-0580 (203) 488-8587 Fax 65-2 North Branford Road Branford, CT 06405 www.CentekEng.com	DATE: 06/30/21 SCALE: AS NOTED JOB NO.: 21022.22					CONDUIT ROUTING AND ELECTRICAL RISER DIAGRAM
REV. 0 DATE 07/23/21 DRAWN BY: BSP CHECK'D BY: TJR CONSTRUCTION DRAWINGS - ISSUED FOR CONSTRUCTION								
E-1							Sheet No. 9 of 11	



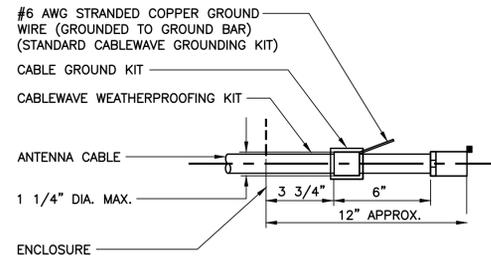
- NOTES:**
- DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO CIGBE

1 CONNECTION OF GROUND WIRES TO GROUND BAR
E-2 SCALE: NOT TO SCALE



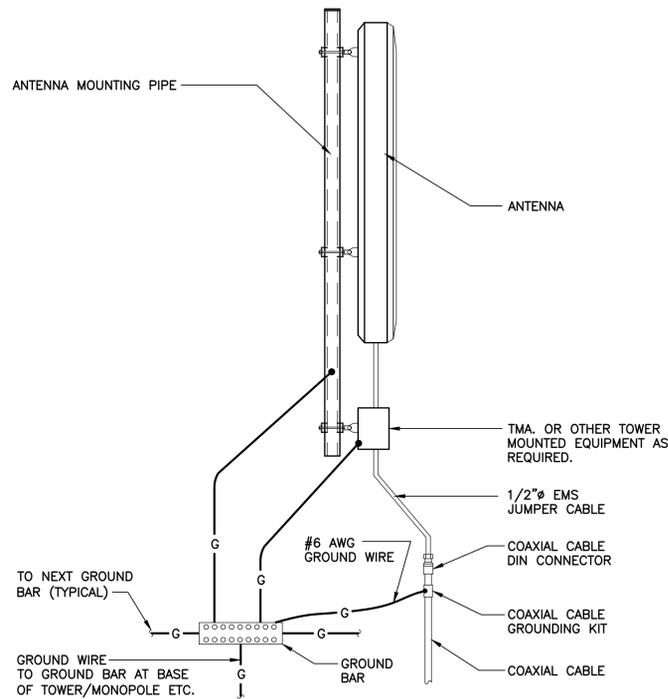
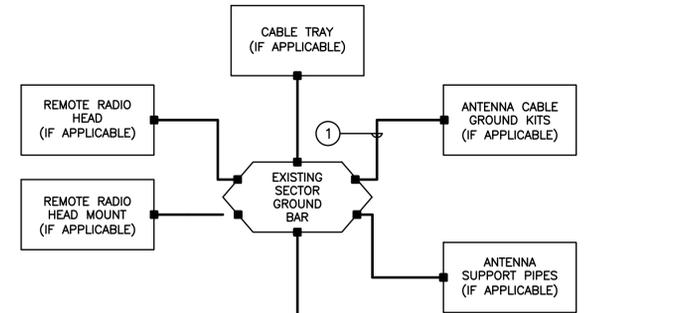
- NOTES**
- TINNED COPPER GROUND BAR, 1/4" x 4" x 20", NEWTON INSTRUMENT CO. HOLE CENTERS TO MATCH NEMA DOUBLE LUG CONFIGURATION.
 - INSULATORS, NEWTON INSTRUMENT CAT. NO. 3061-4.
 - 5/8" LOCK WASHERS, NEWTON INSTRUMENT CO. CAT. NO. 3015-8.
 - WALL MOUNTING BRACKET, NEWTON INSTRUMENT CO. CAT NO. A-6056.
 - 5/8-11 x 1" STAINLESS STEEL TRUSS SPANNER MACHINE SCREWS.

2 GROUND BAR DETAIL
E-2 SCALE: NOT TO SCALE

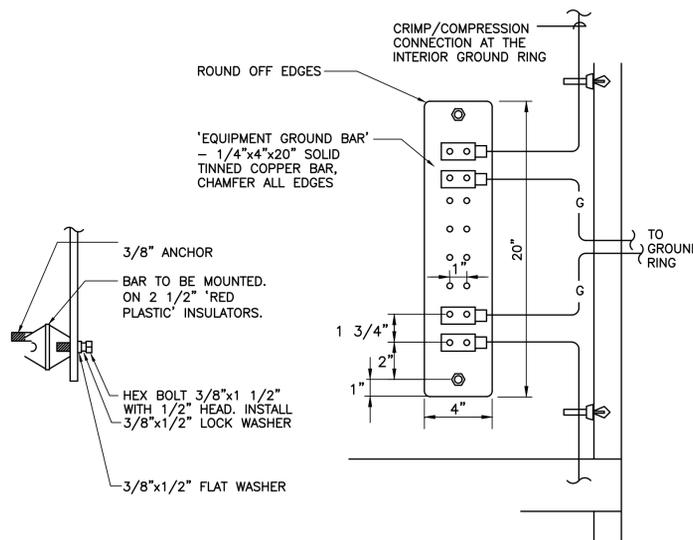


- NOTES:**
- DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO GROUND BAR.

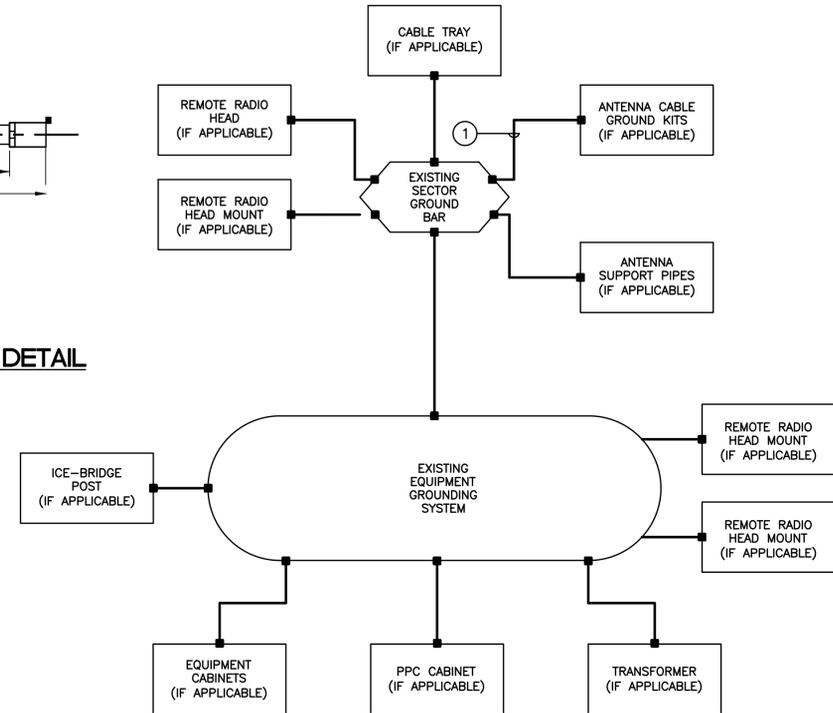
3 ANTENNA CABLE GROUNDING DETAIL
E-2 SCALE: NOT TO SCALE



5 RRH POLE MOUNT GROUNDING
E-2 SCALE: NOT TO SCALE



6 EQUIPMENT GROUND BAR DETAIL
E-2 SCALE: NOT TO SCALE



GROUNDING SCHEMATIC NOTES

- 1 #6 AWG**
- GENERAL NOTES:**
- ALL SURGE SUPPRESSION EQUIPMENT SHALL BE BONDED TO GROUND PER MANUFACTURER'S SPECIFICATIONS
 - UNLESS OTHERWISE NOTED OR REQUIRED BY CODE, GROUND CONDUCTORS SHOWN SHALL BE #2 AWG (SOLID TINNED BCW - EXTERIOR; STRANDED GREEN INSULATED - INTERIOR).
 - BOND CABLE TRAY SECTIONS TOGETHER WITH #6 AWG STRANDED GREEN INSULATED JUMPERS.
 - ALL SECTOR GROUND BARS SHALL BE BONDED TOGETHER WITH #2 AWG SOLID TINNED BCW.
 - BOND ALL EQUIPMENT CABINETS AND BATTERY CABINETS TO GROUND PER MANUFACTURER'S SPECIFICATIONS.
 - REFER TO ALL ELECTRICAL AND GROUNDING DETAILS.
 - COORDINATE ALL ROOF MOUNTED EQUIPMENT WITH OWNER.
 - ALL ROOF MOUNTED AMPLIFIERS AND ASSOCIATED EQUIPMENT SHALL BE BONDED TO THE SECTOR GROUND BAR PER MANUFACTURER'S SPECIFICATIONS.
 - ALL GROUNDING SHALL BE IN ACCORDANCE WITH NEC AND OWNER'S REQUIREMENTS.

7 ELECTRICAL SCHEMATIC DIAGRAM
E-2 SCALE: NOT TO SCALE

PROFESSIONAL ENGINEER SEAL

T-MOBILE

CENTEX engineering
Centered on Solutions
(203) 489-0380 Fax
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65-2 North Branford Road
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T-MOBILE NORTHEAST LLC
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SITE ID: CT11328F
50 MAPLE STREET,
BRANFORD, CT 06405

DATE: 06/30/21
SCALE: AS NOTED
JOB NO. 21022.22

TYPICAL ELECTRICAL DETAILS

E-2

Sheet No. 10 of 11

CONSTRUCTION DRAWINGS - ISSUED FOR CONSTRUCTION

TJR
DATE 07/23/21
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Structural Analysis Report

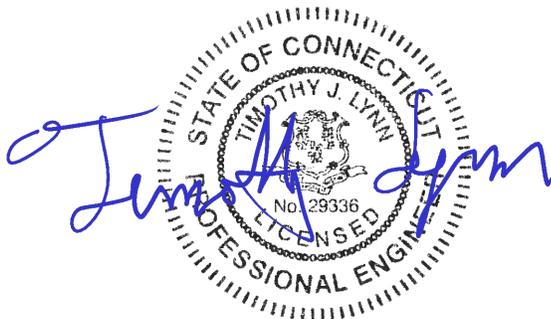
*± 100-ft Existing Masonry Smokestack
& Host Building*

T-Mobile Site Ref: CT11328F

*50 Maple Street
Branford, CT 06405*

Centek Project No. 21022.22

Date: July 6, 2021



Prepared for:
T-Mobile USA
35 Griffin Road
Bloomfield, CT 06002

CENTEK Engineering, Inc.

Structural Analysis – Masonry Smokestack & Host Building

T-Mobile Site Ref ~ CT11328F

Branford, CT

July 6, 2021

Table of Contents

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- INTRODUCTION
- EQUIPMENT INSTALLATION SUMMARY
- DESIGN LOADING
- RESULTS
- CONCLUSION AND RECOMMENDATIONS

SECTION 2 – CONDITIONS & SOFTWARE

- STANDARD ENGINEERING CONDITIONS
- GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM

SECTION 3 – CALCULATIONS

- WIND LOADING
- SMOKESTACK ANALYSIS
- ROOF BEAM – RISA 3D OUTPUT REPORT

SECTION 4 – REFERENCES (NOT ATTACHED)

- RF DATA SHEET, DATED 3/1/2021
- STRUCTURAL ANALYSIS REPORT AS PREPARED BY INTERNATIONAL CHIMNEY CORP., DATED 08/08/2016.

I n t r o d u c t i o n

The purpose of this report is to summarize the results of the structural analysis of the equipment installation proposed by T-Mobile on the existing host masonry smokestack and building located in Branford, CT.

The antennas are mounted on the host ± 100 -ft tall masonry smokestack. The smokestack geometry and structural information was obtained from a field investigation and inspection report prepared by International Chimney Corporation dated August 8, 2016. The equipment cabinets are mounted on the building roof.

P r i m a r y A s s u m p t i o n s U s e d i n t h e A n a l y s i s

- The host structure's theoretical capacity not including any assessment of the condition of the host structure.
- The existing elevated steel antenna frames carry the horizontal and vertical loads due to the weight of equipment, and wind and transfers into host structure.
- Proposed reinforcement and support steel will be properly installed and maintained.
- Structure is in plumb condition.
- Loading for equipment and enclosure as listed in this report.
- All bolts are appropriately tightened providing the necessary connection continuity.
- All welds are fabricated with ER-70S-6 electrodes.
- All members are assumed to be as observed during roof framing mapping.
- All members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.
- All member protective coatings are in good condition.

Antenna and Equipment Summary

Location	Appurtenance / Equipment	Rad Center Elevation (AGL)	Mount Type
Alpha Sector	(2) Ericsson AIR21 antennas (1) RFS-APXVAALL24_43 antenna (1) RFS APX16DWV-16DWVS antenna (1) Ericsson AIR6449 B41 antenna (1) Ericsson 4449 RRU (1) Ericsson 4460 RRU (1) TMA	±96-ft	Antenna mount on smokestack
Beta Sector	(2) Ericsson AIR21 antennas (1) RFS-APXVAALL24_43 antenna (1) RFS APX16DWV-16DWVS antenna (1) Ericsson AIR6449 B41 antenna (1) Ericsson 4449 RRU (1) Ericsson 4460 RRU (1) TMA	±96-ft	Antenna mount on smokestack
Gamma Sector	(2) Ericsson AIR21 antennas (1) RFS-APXVAALL24_43 antenna (1) RFS APX16DWV-16DWVS antenna (1) Ericsson AIR6449 B41 antenna (1) Ericsson 4449 RRU (1) Ericsson 4460 RRU (1) TMA	±96-ft	Antenna mount on smokestack
Equipment Dunnage	(1) Ericsson RBS3106 ±1200 lbs. (1) Ericsson RBS6102 900 lbs. (1) Ericsson B160 1883 lbs. (1) Ericsson 6160 1200 lbs.	- - - -	Steel grating on building roof

Equipment – Indicates equipment to be installed.

~~Equipment~~ – Indicates equipment to be removed.

Analysis

The roof framing was analyzed using a comprehensive computer program titled Risa3D. The program analyzes the equipment platform and antenna mounts considering the worst case code prescribed loading condition. The structures were considered to be loaded by concentric forces, and the model assumes that the members are subjected to bending, axial, and shear forces.

Design Loading

Loading was determined per the requirements of the 2015 International Building Code amended by the 2018 CSBC and ASCE 7-10 “Minimum Design Loads for Buildings and Other Structures”.

Wind Speed:	$V_{ult} = 130$ mph	<i>Appendix N of the 2018 CT State Building Code</i>
Risk Category:	II	<i>2015 IBC; Table 1604.05</i>
Exposure Category:	Surface Roughness C	<i>ASCE 7-10; Section 26.7.2</i>
Ground Snow Load	30 psf	<i>Appendix N of the 2018 CT State Building Code</i>
Dead Load	50psf + equipment and framing self-weight	<i>Identified within SAR design calculations</i>
Live Load	20 psf	<i>ASCE 7-10; Table 4-1 “Roofs – All Other Construction”</i>

Results

Roof Framing:

Component	Stress Ratio (percentage of capacity)	Result
W24 Girder	83%	PASS

Smokestack:

Component	Stress Ratio (percentage of capacity)	Result
Compression	24%	PASS
Tension of Mortar	39%	PASS

CENTEK Engineering, Inc.

Structural Analysis – Masonry Smokestack & Host Building

T-Mobile Site Ref ~ CT11328F

Branford, CT

July 6, 2021

Conclusion

This analysis shows that the subject smokestack and host building **are adequate** to support the proposed T-Mobile equipment installation.

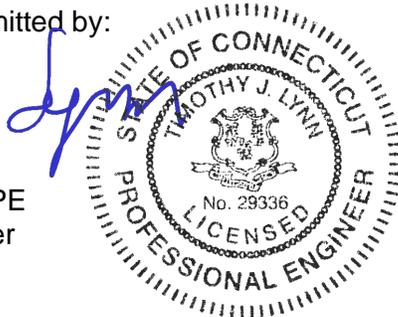
The analysis is based, in part on the information provided to this office by T-Mobile. If the existing conditions are different than the information in this report, CENTEK engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.

Respectfully Submitted by:



Timothy J. Lynn, PE
Structural Engineer



CEN TEK Engineering, Inc.

Structural Analysis – Masonry Smokestack & Host Building

T-Mobile Site Ref ~ CT11328F

Branford, CT

July 6, 2021

*Standard Conditions for Furnishing of
Professional Engineering Services on
Existing Structures*

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil conditions, the antenna and feed line loading on the structure and its components, or other relevant information.
- Information from the field and/or drawings in the possession of Centek Engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to Centek Engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an un-corroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the “as new” condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. Centek Engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

Design Wind Load on Other Structures:

(Based on IBC 2015, CSBC 2018 and ASCE 7-10)

Wind Speed =	$V := 130$ mph	(User Input)	(CSBC Appendix-N)
Risk Category =	$BC := II$	(User Input)	(IBC Table 1604.5)
Exposure Category =	$Exp := C$	(User Input)	
Structure Type =	$Structuretype := Round_Chimney$	(User Input)	
Structure Height =	$Height := 100$ ft	(User Input)	
Horizontal Dimension of Structure =	$Width := 9.5$ ft	(User Input)	
<u>Terrain Exposure Constants:</u>			
Nominal Height of the Atmospheric Boundary Layer =	$z_g := \begin{cases} 1200 & \text{if } Exp = B = 900 \\ 900 & \text{if } Exp = C \\ 700 & \text{if } Exp = D \end{cases}$		(Table 26.9-1)
3-Sec Gust Speed Power Law Exponent =	$\alpha := \begin{cases} 7 & \text{if } Exp = B = 9.5 \\ 9.5 & \text{if } Exp = C \\ 11.5 & \text{if } Exp = D \end{cases}$		(Table 26.9-1)
Integral Length Scale Factor =	$l := \begin{cases} 320 & \text{if } Exp = B = 500 \\ 500 & \text{if } Exp = C \\ 650 & \text{if } Exp = D \end{cases}$		(Table 26.9-1)
Integral Length Scale Power Law Exponent =	$E := \begin{cases} \frac{1}{3} & \text{if } Exp = B = 0.2 \\ \frac{1}{5} & \text{if } Exp = C \\ \frac{1}{8} & \text{if } Exp = D \end{cases}$		(Table 26.9-1)
Turbulence Intensity Factor =	$c := \begin{cases} 0.3 & \text{if } Exp = B = 0.2 \\ 0.2 & \text{if } Exp = C \\ 0.15 & \text{if } Exp = D \end{cases}$		(Table 26.9-1)
Exposure Constant =	$Z_{min} := \begin{cases} 30 & \text{if } Exp = B = 15 \\ 15 & \text{if } Exp = C \\ 7 & \text{if } Exp = D \end{cases}$		(Table 26.9-1)
Topographic Factor =	$K_{zt} := 1$		(Eq. 26.8-2)
Wind Directionality Factor =	$K_d := 0.95$		(Table 26.6-1)
Peak Factor for Background Response =	$g_Q := 3.4$		(Sec 26.9.4)
Peak Factor for Wind Response =	$g_v := 3.4$		(Sec 26.9.4)

Equivalent Height of Structure =

$$z := \begin{cases} Z_{\min} & \text{if } Z_{\min} > 0.6 \cdot \text{Height} \\ 0.6 \cdot \text{Height} & \text{otherwise} \end{cases} = 60 \quad (\text{Sec 26.9.4})$$

Intensity of Turbulence =

$$I_z := c \cdot \left(\frac{33}{z} \right)^{\left(\frac{1}{6} \right)} = 0.181 \quad (\text{Eq. 26.9-7})$$

Integral Length Scale of Turbulence =

$$L_z := l \cdot \left(\frac{z}{33} \right)^E = 563.505 \quad (\text{Eq. 26.9-9})$$

Background Response Factor =

$$Q := \sqrt{\frac{1}{1 + 0.63 \left(\frac{\text{Width} + \text{Height}}{L_z} \right)^{0.63}}} = 0.904 \quad (\text{Eq. 26.9-8})$$

Gust Response Factor =

$$G := 0.925 \cdot \left[\frac{(1 + 1.7 \cdot g_Q \cdot I_z \cdot Q)}{1 + 1.7 \cdot g_V \cdot I_z} \right] = 0.879 \quad (\text{Eq. 26.9-6})$$

Velocity Pressure =

$$q_z := 0.00256 \cdot K_{zt} \cdot K_d \cdot V^2 = 41.1 \quad (\text{Eq. 29.3-1})$$

Force Coefficient =

$$C_f = 0.82 \quad (\text{Fig 29.5-1 - 29.5-3})$$

Ultimate Wind Pressure =

$$F := q_z \cdot G \cdot C_f = 29.6 \quad \text{psf}$$

Height Above Grade =

$$Z := 85 \quad \text{ft} \quad (\text{User Input})$$

Exposure Coefficient =

$$K_z := \begin{cases} 2.01 \left(\frac{Z}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } 15 \leq Z \leq z_g \\ 2.01 \left(\frac{15}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } Z < 15 \end{cases} = 1.22 \quad (\text{Table 29.3-1})$$

$$K_z = 1.223$$

Height Above Grade =

$$Z := 55 \quad \text{ft} \quad (\text{User Input})$$

Exposure Coefficient =

$$K_z := \begin{cases} 2.01 \left(\frac{Z}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } 15 \leq Z \leq z_g \\ 2.01 \left(\frac{15}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } Z < 15 \end{cases} = 1.12 \quad (\text{Table 29.3-1})$$

$$K_z = 1.116$$

Height Above Grade = $Z := 35$ ft (User Input)

Exposure Coefficient = $K_z := \begin{cases} 2.01 \left(\frac{Z}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } 15 \leq Z \leq z_g = 1.01 \\ 2.01 \left(\frac{15}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } Z < 15 \end{cases}$ (Table 29.3-1)

$K_z = 1.015$

Height Above Grade = $Z := 27$ ft (User Input)

Exposure Coefficient = $K_z := \begin{cases} 2.01 \left(\frac{Z}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } 15 \leq Z \leq z_g = 0.96 \\ 2.01 \left(\frac{15}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } Z < 15 \end{cases}$ (Table 29.3-1)

$K_z = 0.961$

Height Above Grade = $Z := 20$ ft (User Input)

Exposure Coefficient = $K_z := \begin{cases} 2.01 \left(\frac{Z}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } 15 \leq Z \leq z_g = 0.9 \\ 2.01 \left(\frac{15}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } Z < 15 \end{cases}$ (Table 29.3-1)

$K_z = 0.902$

Job : CT11328F
 Address: 50 Maple Street Branford, CT 06405
 Description: Smokestack Evaluation

Project No. 21022.22 Sheet 1 of 2
 Computed by TJL Date 7/6/21
 Checked by LAA Date

	Wind Force (lb)	Weight (lb)	Height Above Base (ft)	Height (in)
T-Mobile	2500	1500	96	1152
Sprint	1883	936	88	1056

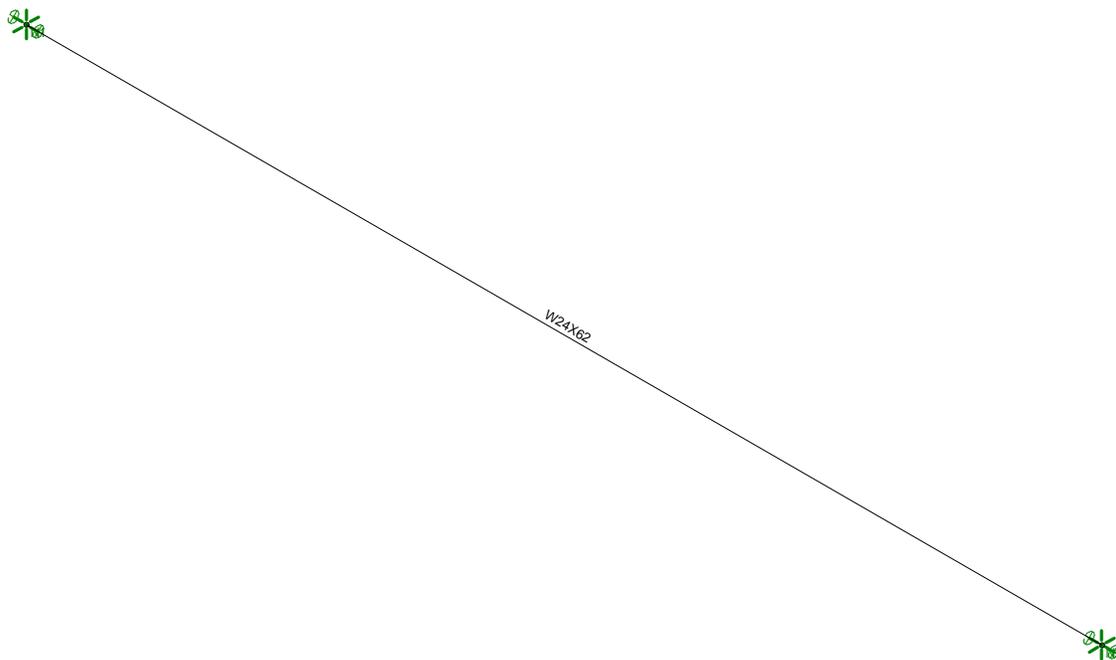
Section	Top Dia (in)	Bot Dia (in)	Wall Thk (in)	Sect Height (in)	Area At Base (in ²)	Tot. Vol (ft ³)	Unit Weight (pcf)	Weight of Section (lb)	Total Weight (lb)	Axial Stress fa (psi)
1	114	135.67	8	356.4	3207.0704	604.97204	127	76831.4485	79267.4485	24.7
2	135.67	161.4	8.5	360	4080.901	778.2026	125	97275.3249	176542.7734	43.3
3	161.4	169.92	9.5	120	4785.3286	323.30268	125	40412.83516	216955.6086	45.3
4	169.92	175.68	10.5	80	5445.9846	247.58964	125	30948.70445	247904.313	45.5
5	175.68	177.96	13	76	6733.6672	293.93989	125	36742.48571	284646.7987	42.3

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 Checked by LAA

Sheet 2 of 2
 Date 7/6/21
 Date

Ultimate Wind Pressure (psf)	ASD Wind Pressure (psf)	KZ	Wind Area (sf)	Wind Force (lb)	Moment @ Base	Section Modulus @ Base	Bending Stress fb (psi)	Allowable Fa (psi)	Allowable Fb (psi)	fa/Fa+fb/Fb		ft	Ft	ft/Ft	
30	18	1.23	309.0	6840.5	3299840.856	96703.96897	34.1	375	500	0.13	OK	9.4	40	0.24	OK
30	18	1.12	371.3	7486.2	8687817.964	148233.9248	58.6	375	500	0.23	OK	15.3	40	0.38	OK
30	18	1.02	138.1	2534.6	11085056.05	181821.2694	61.0	375	500	0.24	OK	15.6	40	0.39	OK
30	18	0.096	96.0	165.9	12791234.22	212305.0695	60.2	375	500	0.24	OK	14.7	40	0.37	OK
0	0	0	93.3	0.0	14418407.22	259009.3359	55.7	375	500	0.22	OK	13.4	40	0.33	OK

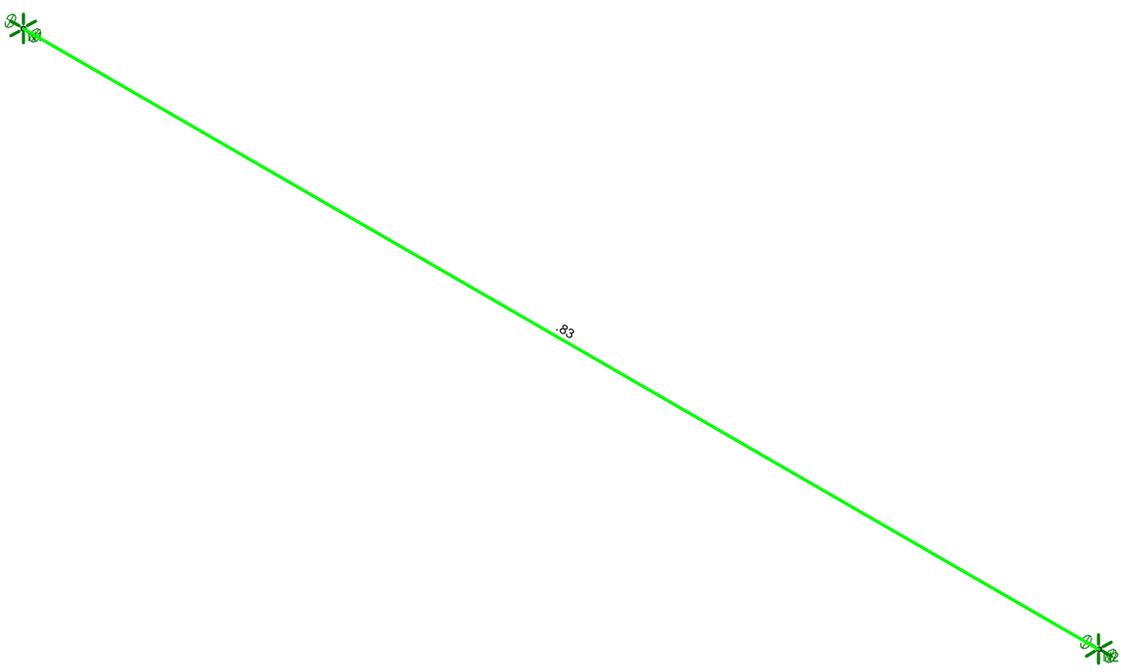


Envelope Only Solution

Centek Engineering	CT11328 Roof Member Analysis Member Framing	July 6, 2021 at 3:27 PM
TJL		Existing W24 Analysis.r3d
21022.22		



Code Check (Env)	
Black	No Calc
Red	> 1.0
Magenta	.90-1.0
Green	.75-.90
Cyan	.50-.75
Blue	0-.50



Member Code Checks Displayed (Enveloped)
Envelope Only Solution

Centek Engineering	CT11328 Roof Member Analysis Unity Check	
TJL		July 6, 2021 at 3:27 PM
21022.22		Existing W24 Analysis.r3d

(Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (ft/sec^2)	32.2
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver

Hot Rolled Steel Code	AISC 14th(360-10): ASD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 14th(360-10): ASD
Cold Formed Steel Code	AISI S100-10: ASD
Wood Code	AWC NDS-12: ASD
Wood Temperature	< 100F
Concrete Code	ACI 318-11
Masonry Code	ACI 530-11: ASD
Aluminum Code	AA ADM1-10: ASD - Building
Stainless Steel Code	AISC 14th(360-10): ASD
Adjust Stiffness?	Yes(Iterative)

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	Yes
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8

(Global) Model Settings, Continued

Seismic Code	ASCE 7-10
Seismic Base Elevation (ft)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
R X	3
R Z	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	I or II
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	4
Cd X	4
Rho Z	1
Rho X	1
Footing Overturning Safety Factor	1
Optimize for OTM/Sliding	No
Check Concrete Bearing	No
Footing Concrete Weight (k/ft^3)	150.001
Footing Concrete f'c (ksi)	4
Footing Concrete Ec (ksi)	3644
Lambda	1
Footing Steel fy (ksi)	60
Minimum Steel	0.0018
Maximum Steel	0.0075
Footing Top Bar	#3
Footing Top Bar Cover (in)	2
Footing Bottom Bar	#3
Footing Bottom Bar Cover (in)	3.5
Pedestal Bar	#3
Pedestal Bar Cover (in)	1.5
Pedestal Ties	#3

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (\... Density[k/ft^3]	Yield[ksi]	Ry	Fu[ksi]	Rt	
1	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	58	1.2
3	A992	29000	11154	.3	.65	.49	50	1.1	58	1.2
4	A500 Gr.42	29000	11154	.3	.65	.49	42	1.3	58	1.1
5	A500 Gr.46	29000	11154	.3	.65	.49	46	1.2	58	1.1
6	A53 Grade B	29000	11154	.3	.65	.49	35	1.5	58	1.2

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Ru... A [in ²]	Iyy [in ⁴]	Izz [in ⁴]	J [in ⁴]
1	W24x62	W24X62	Column	Wide Flange	A36 Gr.36	Typical	18.2	34.5	1550 1.71

Hot Rolled Steel Design Parameters

	Label	Shape	Length[ft]	Lbyy[ft]	Lbzz[ft]	Lcomp top[...Lcomp bot[...L-torq...	Kyy	Kzz	Cb	Funci...
1	M1	W24x62	32			4				Lateral

Member Primary Data

	Label	I Joint	J Joint	K Joint	Rotate(...	Section/Shape	Type	Design List	Material	Design R...
1	M1	N1	N2			W24x62	Column	Wide Flange	A36 Gr.36	Typical

Joint Coordinates and Temperatures

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Diap...
1	N1	0	0	0	0	
2	N2	32	0	0	0	

Joint Boundary Conditions

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
1	N2	Reaction	Reaction	Reaction	Reaction		
2	N1	Reaction	Reaction	Reaction	Reaction		

Member Point Loads (BLC 2 : Weight of Equipment)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M1	Y	-1	7
2	M1	Y	-1	11
3	M1	Y	-1.2	16
4	M1	Y	-1.9	20

Member Distributed Loads (BLC 2 : Weight of Equipment)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/f...	Start Location[ft,%]	End Location[ft,%]
1	M1	Y	-.06	-.06	5.5	26.5

Member Distributed Loads (BLC 3 : Dead Load)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/f...	Start Location[ft,%]	End Location[ft,%]
1	M1	Y	-1.1	-1.1	0	9
2	M1	Y	-.8	-.8	9	23
3	M1	Y	-1.1	-1.1	23	32

Member Distributed Loads (BLC 4 : Snow Load)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/f...	Start Location[ft,%]	End Location[ft,%]
1	M1	Y	-.66	-.66	0	9
2	M1	Y	-.48	-.48	9	23



Member Distributed Loads (BLC 4 : Snow Load) (Continued)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/f...	Start Location[ft,%]	End Location[ft,%]
3	M1	Y	-66	-66	23	32

Member Distributed Loads (BLC 5 : Roof Live Load)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/f...	Start Location[ft,%]	End Location[ft,%]
1	M1	Y	-44	-44	0	9
2	M1	Y	-32	-32	9	23
3	M1	Y	-44	-44	23	32

Basic Load Cases

	BLC Description	Category	X Gra...	Y Gra...	Z Gra...	Joint	Point	Distrib..	Area(... Surfa...
1	Self Weight	DL		-1					
2	Weight of Equipment	DL					4	1	
3	Dead Load	DL						3	
4	Snow Load	SL						3	
5	Roof Live Load	RLL						3	

Load Combinations

	Description	Solve	P...	S...	B...	Fa...	BLC	Fact...	BLC Fa...	BLC Fa...	BLC Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	IBC 16-8	Yes	Y		DL	1													
2	IBC 16-9	Yes	Y		DL	1	LL	1	LLS	1									
3	IBC 16-10 (a)	Yes	Y		DL	1	RLL	1											
4	IBC 16-10 (b)	Yes	Y		DL	1	SL	1	SLN	1									
5	IBC 16-10 (c)	Yes	Y		DL	1	RL	1											
6	IBC 16-11 (a)	Yes	Y		DL	1	LL	.75	LLS	.75	RLL	.75							
7	IBC 16-11 (b)	Yes	Y		DL	1	LL	.75	LLS	.75	SL	.75	SLN	.75					
8	IBC 16-11 (c)	Yes	Y		DL	1	LL	.75	LLS	.75	RL	.75							
9	IBC 16-12 (a) (a)	Yes	Y		DL	1	WLX	.6											
10	IBC 16-12 (a) (b)	Yes	Y		DL	1	WLZ	.6											
11	IBC 16-12 (a) (c)	Yes	Y		DL	1	WLX	-.6											
12	IBC 16-12 (a) (d)	Yes	Y		DL	1	WLZ	-.6											
13	IBC 16-13 (a) (a)	Yes	Y		DL	1	WLX	.45	LL	.75	LLS	.75	RLL	.75					
14	IBC 16-13 (a) (b)	Yes	Y		DL	1	WLZ	.45	LL	.75	LLS	.75	RLL	.75					
15	IBC 16-13 (a) (c)	Yes	Y		DL	1	WLX	-.45	LL	.75	LLS	.75	RLL	.75					
16	IBC 16-13 (a) (d)	Yes	Y		DL	1	WLZ	-.45	LL	.75	LLS	.75	RLL	.75					
17	IBC 16-13 (b) (a)	Yes	Y		DL	1	WLX	.45	LL	.75	LLS	.75	SL	.75	S...	.75			
18	IBC 16-13 (b) (b)	Yes	Y		DL	1	WLZ	.45	LL	.75	LLS	.75	SL	.75	S...	.75			
19	IBC 16-13 (b) (c)	Yes	Y		DL	1	WLX	-.45	LL	.75	LLS	.75	SL	.75	S...	.75			
20	IBC 16-13 (b) (d)	Yes	Y		DL	1	WLZ	-.45	LL	.75	LLS	.75	SL	.75	S...	.75			
21	IBC 16-13 (c) (a)	Yes	Y		DL	1	WLX	.45	LL	.75	LLS	.75	RL	.75					
22	IBC 16-13 (c) (b)	Yes	Y		DL	1	WLZ	.45	LL	.75	LLS	.75	RL	.75					
23	IBC 16-13 (c) (c)	Yes	Y		DL	1	WLX	-.45	LL	.75	LLS	.75	RL	.75					
24	IBC 16-13 (c) (d)	Yes	Y		DL	1	WLZ	-.45	LL	.75	LLS	.75	RL	.75					
25	IBC 16-15 (a)	Yes	Y		DL	.6	WLX	.6											
26	IBC 16-15 (b)	Yes	Y		DL	.6	WLZ	.6											
27	IBC 16-15 (c)	Yes	Y		DL	.6	WLX	-.6											
28	IBC 16-15 (d)	Yes	Y		DL	.6	WLZ	-.6											



Envelope Joint Reactions

	Joint		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N2	max	0	28	28.771	4	0	28	0	28	0	28	0	28
2		min	0	1	11.683	25	0	1	0	1	0	1	0	1
3	N1	max	0	28	29.171	4	0	28	0	28	0	28	0	28
4		min	0	1	11.923	25	0	1	0	1	0	1	0	1
5	Totals:	max	0	28	57.942	4	0	28						
6		min	0	1	23.605	25	0	1						

Envelope Joint Displacements

	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotatio...	LC	Z Rotation [rad]	LC
1	N1	max	0	28	0	28	0	28	0	28	0	28	-4.087e-03	28
2		min	0	1	0	1	0	1	0	1	0	1	-9.815e-03	4
3	N2	max	0	28	0	28	0	28	0	28	0	28	9.777e-03	4
4		min	0	1	0	1	0	1	0	1	0	1	4.064e-03	25

Envelope AISC 14th(360-10): ASD Steel Code Checks

Member	Shape	Code Check	Lo...	LC	She...Lo...	Dir	...Pnc/...Pnt/o...	Mny...	Mnz...	Cb	Eqn
1	M1	W24X62	.829	16	4	.199 0	y 4	35.167392...	28.171274.85	1	H1-...

Structural Analysis Report

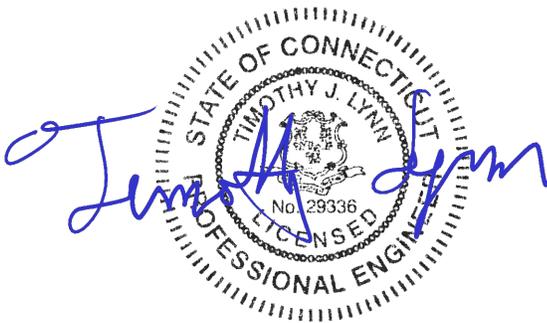
Antenna Mount Analysis

T-Mobile Site #: CT11328F

*50 Maple Street
Branford, CT*

Centek Project No. 21022.22

Date: July 6, 2021



Prepared for:
T-Mobile USA
35 Griffin Road
Bloomfield, CT 06002

CENTEK Engineering, Inc.
Structural Analysis – Mount Analysis
T-Mobile Site Ref. ~ CT11328F
Branford, CT
July 6, 2021

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- ANTENNA AND APPURTENANCE SUMMARY
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SECTION 3 – REFERENCE MATERIALS (NOT INCLUDED WITHIN REPORT)

- RF DATA SHEET, DATED 6/15/2021

July 6, 2021

Mr. Dan Reid
Transcend Wireless
10 Industrial Ave
Mahwah, NJ 07430

Re: *Structural Letter ~ Antenna Mount*
T-Mobile – Site Ref: CT11328F
50 Maple Street
Branford, CT 06405

Centek Project No. 21022.22

Dear Mr. Reid,

Centek Engineering, Inc. has reviewed the T-Mobile antenna installation at the above referenced site. The purpose of the review is to determine the structural adequacy of the existing mount, consisting three (3) sector mounts with stiff arms to support the proposed/existing equipment configuration. The review considered the effects of wind load, dead load and ice load in accordance with the 2015 International Building Code as modified by the 2018 Connecticut State Building Code (CTBC) and ASCE 7-10.

The loads considered in this analysis consist of the following:

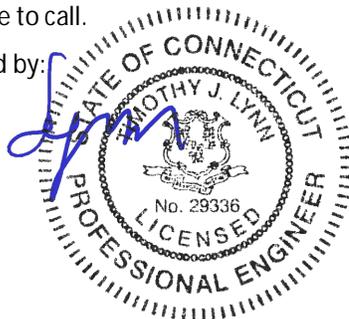
- T-Mobile:
Sector Frames: Three (3) RFS APXVAALL24_43 panel antennas, three (3) Ericsson AIR6449 panel antennas, three (3) RFS APX16DWV-16DWVS panel antennas, three (3) Ericsson 4449 remote radio units and three (3) Ericsson 4460 remote radio units mounted on three (3) sector frames with a RAD center elevation of 96-ft +/- AGL.

The antenna mount was analyzed per the requirements of the 2015 International Building Code as modified by the 2018 Connecticut State Building Code considering an ultimate design wind speed of 130 mph for Branford as required in Appendix N of the 2018 Connecticut State Building Code.

Based on our review of the installation, it is our opinion that the subject antenna mount has sufficient capacity to support the aforementioned antenna configuration. If there are any questions regarding this matter, please feel free to call.

Respectfully Submitted by:


Timothy J. Lynn, PE
Structural Engineer



CEN TEK Engineering, Inc.
Structural Analysis – Mount Analysis
T-Mobile Site Ref. ~ CT11328F
Branford, CT
July 6, 2021

Section 2 - Calculations

Design Wind Load on Other Structures:

(Based on IBC 2015, CSBC 2018 and ASCE 7-10)

Wind Speed =	V := 130	mph	(User Input)	(CSBC Appendix-N)
Risk Category =	BC := II		(User Input)	(IBC Table 1604.5)
Exposure Category =	Exp := C		(User Input)	
Height Above Grade =	Z := 96	ft	(User Input)	
Structure Type =	Structuretype :=	Square_Chimney	(User Input)	
Structure Height =	Height := 8	ft	(User Input)	
Horizontal Dimension of Structure =	Width := 2	ft	(User Input)	

Terrain Exposure Constants:

Nominal Height of the Atmospheric Boundary Layer =

$$z_g := \begin{cases} 1200 & \text{if } \text{Exp} = \text{B} = 900 \\ 900 & \text{if } \text{Exp} = \text{C} \\ 700 & \text{if } \text{Exp} = \text{D} \end{cases} \quad \text{(Table 26.9-1)}$$

3-Sec Gust Speed Power Law Exponent =

$$\alpha := \begin{cases} 7 & \text{if } \text{Exp} = \text{B} = 9.5 \\ 9.5 & \text{if } \text{Exp} = \text{C} \\ 11.5 & \text{if } \text{Exp} = \text{D} \end{cases} \quad \text{(Table 26.9-1)}$$

Integral Length Scale Factor =

$$l := \begin{cases} 320 & \text{if } \text{Exp} = \text{B} = 500 \\ 500 & \text{if } \text{Exp} = \text{C} \\ 650 & \text{if } \text{Exp} = \text{D} \end{cases} \quad \text{(Table 26.9-1)}$$

Integral Length Scale Power Law Exponent =

$$E := \begin{cases} \frac{1}{3} & \text{if } \text{Exp} = \text{B} = 0.2 \\ \frac{1}{5} & \text{if } \text{Exp} = \text{C} \\ \frac{1}{8} & \text{if } \text{Exp} = \text{D} \end{cases} \quad \text{(Table 26.9-1)}$$

Turbulence Intensity Factor =

$$c := \begin{cases} 0.3 & \text{if } \text{Exp} = \text{B} = 0.2 \\ 0.2 & \text{if } \text{Exp} = \text{C} \\ 0.15 & \text{if } \text{Exp} = \text{D} \end{cases} \quad \text{(Table 26.9-1)}$$

Exposure Constant =

$$Z_{\min} := \begin{cases} 30 & \text{if } \text{Exp} = \text{B} = 15 \\ 15 & \text{if } \text{Exp} = \text{C} \\ 7 & \text{if } \text{Exp} = \text{D} \end{cases} \quad \text{(Table 26.9-1)}$$

Exposure Coefficient =

$$K_z := \begin{cases} 2.01 \left(\frac{Z}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } 15 \leq Z \leq z_g = 1.25 \\ 2.01 \left(\frac{15}{z_g} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if } Z < 15 \end{cases} \quad \text{(Table 29.3-1)}$$

Topographic Factor =	$K_{zt} := 1$	(Eq. 26.8-2)
Wind Directionality Factor =	$K_d = 0.9$	(Table 26.6-1)
Velocity Pressure =	$q_z := 0.00256 \cdot K_z \cdot K_{zt} \cdot K_d \cdot V^2 = 48.86$	(Eq. 29.3-1)
Peak Factor for Background Response =	$g_Q := 3.4$	(Sec 26.9.4)
Peak Factor for Wind Response =	$g_V := 3.4$	(Sec 26.9.4)
Equivalent Height of Structure =	$z := \begin{cases} Z_{\min} & \text{if } Z_{\min} > 0.6 \cdot \text{Height} \\ 0.6 \cdot \text{Height} & \text{otherwise} \end{cases} = 15$	(Sec 26.9.4)
Intensity of Turbulence =	$I_z := c \cdot \left(\frac{33}{z}\right)^{\left(\frac{1}{6}\right)} = 0.228$	(Eq. 26.9-7)
Integral Length Scale of Turbulence =	$L_Z := l \cdot \left(\frac{z}{33}\right)^E = 427.057$	(Eq. 26.9-9)
Background Response Factor =	$Q := \sqrt{\frac{1}{1 + 0.63 \left(\frac{\text{Width} + \text{Height}}{L_Z}\right)^{0.63}}} = 0.972$	(Eq. 26.9-8)
Gust Response Factor =	$G := 0.925 \cdot \left[\frac{(1 + 1.7 \cdot g_Q \cdot I_z \cdot Q)}{1 + 1.7 \cdot g_V \cdot I_z} \right] = 0.91$	(Eq. 26.9-6)
Force Coefficient =	$C_f = 1.35$	(Fig 29.5-1 - 29.5-3)

Wind Force =

$F := q_z \cdot G \cdot C_f = 60$

psf

Development of Wind & Ice Load on Antennas

Antenna Data:

Antenna Model =	RFSAPX16DWV-16DWVS	
Antenna Shape =	Flat	(User Input)
Antenna Height =	$L_{ant} := 55.9$	in (User Input)
Antenna Width =	$W_{ant} := 13$	in (User Input)
Antenna Thickness =	$T_{ant} := 3.15$	in (User Input)
Antenna Weight =	$WT_{ant} := 45$	lbs (User Input)
Number of Antennas =	$N_{ant} := 1$	(User Input)

Wind Load (Front)

Surface Area for One Antenna =	$SA_{ant} := \frac{L_{ant} \cdot W_{ant}}{144} = 5$	sf
Antenna Projected Surface Area =	$A_{ant} := SA_{ant} \cdot N_{ant} = 5$	sf
Total Antenna Wind Force =	$F_{ant} := F \cdot A_{ant} = 303$	lbs

Wind Load (Side)

Surface Area for One Antenna =	$SA_{ant} := \frac{L_{ant} \cdot T_{ant}}{144} = 1.2$	sf
Antenna Projected Surface Area =	$A_{ant} := SA_{ant} \cdot N_{ant} = 1.2$	sf
Total Antenna Wind Force =	$F_{ant} := F \cdot A_{ant} = 73$	lbs

Gravity Load (without ice)

Weight of All Antennas =	$WT_{ant} \cdot N_{ant} = 45$	lbs
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Development of Wind & Ice Load on Antennas

Antenna Data:

Antenna Model =	RFSAPXVAALL24-43	
Antenna Shape =	Flat	(User Input)
Antenna Height =	$L_{ant} := 95.9$	in (User Input)
Antenna Width =	$W_{ant} := 24$	in (User Input)
Antenna Thickness =	$T_{ant} := 8.5$	in (User Input)
Antenna Weight =	$WT_{ant} := 150$	lbs (User Input)
Number of Antennas =	$N_{ant} := 1$	(User Input)

Wind Load (Front)

Surface Area for One Antenna =	$SA_{ant} := \frac{L_{ant} \cdot W_{ant}}{144} = 16$	sf
Antenna Projected Surface Area =	$A_{ant} := SA_{ant} \cdot N_{ant} = 16$	sf
Total Antenna Wind Force =	$F_{ant} := F \cdot A_{ant} = 959$	lbs

Wind Load (Side)

Surface Area for One Antenna =	$SA_{ant} := \frac{L_{ant} \cdot T_{ant}}{144} = 5.7$	sf
Antenna Projected Surface Area =	$A_{ant} := SA_{ant} \cdot N_{ant} = 5.7$	sf
Total Antenna Wind Force =	$F_{ant} := F \cdot A_{ant} = 340$	lbs

Gravity Load (without ice)

Weight of All Antennas =	$WT_{ant} \cdot N_{ant} = 150$	lbs
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Development of Wind & Ice Load on Antennas

Antenna Model =	Ericsson AIR6449	
Antenna Shape =	Flat	(User Input)
Antenna Height =	$L_{ant} := 33.1$	in (User Input)
Antenna Width =	$W_{ant} := 20.5$	in (User Input)
Antenna Thickness =	$T_{ant} := 8.3$	in (User Input)
Antenna Weight =	$WT_{ant} := 103$	lbs (User Input)
Number of Antennas =	$N_{ant} := 1$	(User Input)

Wind Load (Front)

Surface Area for One Antenna =	$SA_{ant} := \frac{L_{ant} \cdot W_{ant}}{144} = 4.7$	sf
Antenna Projected Surface Area =	$A_{ant} := SA_{ant} \cdot N_{ant} = 4.7$	sf
Total Antenna Wind Force =	$F_{ant} := F \cdot A_{ant} = 283$	lbs

Wind Load (Side)

Surface Area for One Antenna =	$SA_{ant} := \frac{L_{ant} \cdot T_{ant}}{144} = 1.9$	sf
Antenna Projected Surface Area =	$A_{ant} := SA_{ant} \cdot N_{ant} = 1.9$	sf
Total Antenna Wind Force =	$F_{ant} := F \cdot A_{ant} = 115$	lbs

Gravity Load (without ice)

Weight of All Antennas =	$WT_{ant} \cdot N_{ant} = 103$	lbs
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Development of Wind & Ice Load on RRHs

RRUS Data:

RRUS Model =	Ericsson 4449	
RRUS Shape =	Flat	(User Input)
RRUS Height =	$L_{RRH} := 14.9$	in (User Input)
RRUS Width =	$W_{RRH} := 13.2$	in (User Input)
RRUS Thickness =	$T_{RRH} := 10.4$	in (User Input)
RRUS Weight =	$W_{T_{RRH}} := 74$	lbs (User Input)
Number of RRUSs =	$N_{RRH} := 1$	(User Input)

Wind Load (Front)

Surface Area for One RRH =	$SA_{RRH} := \frac{L_{RRH} \cdot W_{RRH}}{144} = 1.4$	sf
RRH Projected Surface Area =	$A_{RRH} := SA_{RRH} \cdot N_{RRH} = 1.4$	sf
Total RRH Wind Force =	$F_{RRH} := F \cdot A_{RRH} = 82$	lbs

Wind Load (Side)

Surface Area for One RRH =	$SA_{RRH} := \frac{L_{RRH} \cdot T_{RRH}}{144} = 1.1$	sf
RRH Projected Surface Area =	$A_{RRH} := SA_{RRH} \cdot N_{RRH} = 1.1$	sf
Total RRH Wind Force =	$F_{RRH} := F \cdot A_{RRH} = 65$	lbs

Gravity Load (without ice)

Weight of All RRHs =	$W_{T_{RRH}} \cdot N_{RRH} = 74$	lbs
-----------------------------	--	------------

Development of Wind & Ice Load on RRHs

RRUS Data:

RRUS Model =	Ericsson 4460	
RRUS Shape =	Flat	(User Input)
RRUS Height =	$L_{RRH} := 19.6$	in (User Input)
RRUS Width =	$W_{RRH} := 15.7$	in (User Input)
RRUS Thickness =	$T_{RRH} := 12.1$	in (User Input)
RRUS Weight =	$W_{T_{RRH}} := 109$	lbs (User Input)
Number of RRUSs =	$N_{RRH} := 1$	(User Input)

Wind Load (Front)

Surface Area for One RRH =	$SA_{RRH} := \frac{L_{RRH} \cdot W_{RRH}}{144} = 2.1$	sf
RRH Projected Surface Area =	$A_{RRH} := SA_{RRH} \cdot N_{RRH} = 2.1$	sf
Total RRH Wind Force =	$F_{RRH} := F \cdot A_{RRH} = 128$	lbs

Wind Load (Side)

Surface Area for One RRH =	$SA_{RRH} := \frac{L_{RRH} \cdot T_{RRH}}{144} = 1.6$	sf
RRH Projected Surface Area =	$A_{RRH} := SA_{RRH} \cdot N_{RRH} = 1.6$	sf
Total RRH Wind Force =	$F_{RRH} := F \cdot A_{RRH} = 99$	lbs

Gravity Load (without ice)

Weight of All RRHs =	$W_{T_{RRH}} \cdot N_{RRH} = 109$	lbs
-----------------------------	---	-----

(Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (ft/sec^2)	32.2
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Y
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver

Hot Rolled Steel Code	AISC 14th(360-10): ASD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 14th(360-10): ASD
Cold Formed Steel Code	AISI S100-12: ASD
Wood Code	AWC NDS-15: ASD
Wood Temperature	< 100F
Concrete Code	ACI 318-14
Masonry Code	ACI 530-13: ASD
Aluminum Code	AA ADM1-15: ASD - Building
Stainless Steel Code	AISC 14th(360-10): ASD
Adjust Stiffness?	Yes(Iterative)

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8

(Global) Model Settings, Continued

Seismic Code	ASCE 7-10
Seismic Base Elevation (ft)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
T Z (sec)	Not Entered
R X	3
R Z	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	I or II
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	4
Cd X	4
Rho Z	1
Rho X	1
Footing Overturning Safety Factor	1
Optimize for OTM/Sliding	No
Check Concrete Bearing	No
Footing Concrete Weight (k/ft^3)	150.001
Footing Concrete f'c (ksi)	4
Footing Concrete Ec (ksi)	3644
Lambda	1
Footing Steel fy (ksi)	60
Minimum Steel	0.0018
Maximum Steel	0.0075
Footing Top Bar	#3
Footing Top Bar Cover (in)	2
Footing Bottom Bar	#3
Footing Bottom Bar Cover (in)	3.5
Pedestal Bar	#3
Pedestal Bar Cover (in)	1.5
Pedestal Ties	#3

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (\... Density[k/ft^3]	Yield[ksi]	Ry	Fu[ksi]	Rt	
1	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	58	1.2
3	A992	29000	11154	.3	.65	.49	50	1.1	58	1.2
4	A500 Gr.42	29000	11154	.3	.65	.49	42	1.3	58	1.1
5	A500 Gr.46	29000	11154	.3	.65	.49	46	1.2	58	1.1
6	A53 Grade B	29000	11154	.3	.65	.49	35	1.5	58	1.2

Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design Ru... A [in ²]	I _{yy} [in ⁴]	I _{zz} [in ⁴]	J [in ⁴]	
1	Pipe 2.0	PIPE_2.0	Beam	Pipe	A53 Grade B	Typical	1.02	.627	.627	1.25
2	Antenna Mast	PIPE_2.0	Column	Pipe	A53 Grade B	Typical	1.02	.627	.627	1.25
3	Horizontal	PIPE_2.0	Beam	Pipe	A53 Grade B	Typical	1.02	.627	.627	1.25

Hot Rolled Steel Design Parameters

	Label	Shape	Length[ft]	L _{byy} [ft]	L _{bzz} [ft]	L _{comp top} [...]	L _{comp bot} [...]	L-torq...	K _{yy}	K _{zz}	C _b	Functi...
1	M1	Antenna Mast	11.667			L _{byy}			Segm...			Lateral
2	M2	Horizontal	9.5			L _{byy}			6			Lateral
3	M3	Antenna Mast	8			L _{byy}						Lateral
4	M4	Antenna Mast	8			L _{byy}						Lateral
5	M5	Horizontal	9.5			L _{byy}			6			Lateral
6	M6	Pipe 2.0	8.998			L _{byy}						Lateral
7	M7	Pipe 2.0	8.998			L _{byy}						Lateral
8	M8	Antenna Mast	9			L _{byy}						Lateral

Member Primary Data

	Label	I Joint	J Joint	K Joint	Rotate(...)	Section/Shape	Type	Design List	Material	Design R...
1	M1	N1	N2			Antenna Mast	Column	Pipe	A53 Grade B	Typical
2	M2	N4	N3			Horizontal	Beam	Pipe	A53 Grade B	Typical
3	M3	N8	N10			Antenna Mast	Column	Pipe	A53 Grade B	Typical
4	M4	N7	N9			Antenna Mast	Column	Pipe	A53 Grade B	Typical
5	M5	N13	N12			Horizontal	Beam	Pipe	A53 Grade B	Typical
6	M6	N6	N18			Pipe 2.0	Beam	Pipe	A53 Grade B	Typical
7	M7	N5	N17			Pipe 2.0	Beam	Pipe	A53 Grade B	Typical
8	M8	N19	N20			Antenna Mast	Column	Pipe	A53 Grade B	Typical
9	M9	N21	N23			RIGID	None	None	RIGID	Typical
10	M10	N22	N24			RIGID	None	None	RIGID	Typical

Joint Coordinates and Temperatures

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Diap...
1	N1	0	5.833333	3.416667	0	
2	N2	0	-5.833333	3.416667	0	
3	N3	4.75	1.5	3	0	
4	N4	-4.75	1.5	3	0	
5	N5	4.166667	1.5	3	0	
6	N6	-4.166667	1.5	3	0	
7	N7	4.166667	-4	3	0	
8	N8	-4.166667	-4	3	0	
9	N9	4.166667	4	3	0	
10	N10	-4.166667	4	3	0	
11	N11	0	1.5	3	0	
12	N12	4.75	-1.5	3	0	
13	N13	-4.75	-1.5	3	0	
14	N14	4.166667	-1.5	3	0	
15	N15	-4.166667	-1.5	3	0	
16	N16	0	-1.5	3	0	

Joint Coordinates and Temperatures (Continued)

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Diap...
17	N17	8.666667	1.5	-4.791667	0	
18	N18	-8.666667	1.5	-4.791667	0	
19	N19	0.	-4.5	3	0	
20	N20	0.	4.5	3	0	
21	N21	0	2.5	3	0	
22	N22	0	-2.5	3	0	
23	N23	0	2.5	3.416667	0	
24	N24	0	-2.5	3.416667	0	

Joint Boundary Conditions

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
1	N11	Reaction	Reaction	Reaction			
2	N16	Reaction	Reaction	Reaction			
3	N18	Reaction	Reaction	Reaction			
4	N17	Reaction	Reaction	Reaction			
5	N21						
6	N22						
7	N23						
8	N24						

Member Point Loads (BLC 2 : Weight of Equipment)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M4	Y	-.052	7.5
2	M4	Y	-.052	3.5
3	M3	Y	-.023	7.5
4	M3	Y	-.023	3.5
5	M3	Y	-.109	1
6	M1	Y	-.075	.5
7	M1	Y	-.075	7.5
8	M1	Y	-.074	5

Member Point Loads (BLC 3 : Wind Load X)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M4	X	.058	7.5
2	M4	X	.058	3.5
3	M3	X	.037	7.5
4	M3	X	.037	3.5
5	M3	X	.099	1
6	M1	X	.17	.5
7	M1	X	.17	7.5
8	M1	X	.065	4

Member Point Loads (BLC 4 : Wind Load Z)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M4	Z	.142	7.5
2	M4	Z	.142	3.5
3	M3	Z	.152	7.5
4	M3	Z	.152	3.5

Member Point Loads (BLC 4 : Wind Load Z) (Continued)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
5	M3	Z	.128	1
6	M1	Z	.48	.5
7	M1	Z	.48	7.5
8	M1	Z	.082	4

Member Distributed Loads (BLC 3 : Wind Load X)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/f...]	Start Location[ft,%]	End Location[ft,%]
1	M6	X	.007	.007	0	0
2	M7	X	.007	.007	0	0
3	M1	X	.007	.007	0	0
4	M3	X	.007	.007	0	0
5	M4	X	.007	.007	0	0
6	M8	X	.007	.007	0	0

Member Distributed Loads (BLC 4 : Wind Load Z)

	Member Label	Direction	Start Magnitude[k/ft,F,ksf]	End Magnitude[k/f...]	Start Location[ft,%]	End Location[ft,%]
1	M2	Z	.007	.007	0	0
2	M5	Z	.007	.007	0	0
3	M3	Z	.007	.007	0	3.308
4	M4	Z	.007	.007	0	3.308
5	M1	Z	.007	.007	8	11.667

Basic Load Cases

	BLC Description	Category	X Gra...	Y Gra...	Z Gra...	Joint	Point	Distrib..	Area(... Surfa...
1	Self Weight	DL		-1					
2	Weight of Equipment	DL					8		
3	Wind Load X	WLX					8	6	
4	Wind Load Z	WLZ					8	5	

Load Combinations

	Description	Solve	P...	S...	B...	Fa...	BLC Fact...	BLC Fa...	BLC Fa...	BLC Fa...	B...	Fa...	B...	Fa...	B...	Fa...	B...	Fa...
1	IBC 16-8	Yes	Y		DL	1												
2	IBC 16-9	Yes	Y		DL	1	LL	1	LLS	1								
3	IBC 16-12 (a) (a)	Yes	Y		DL	1	WLX	.6										
4	IBC 16-12 (a) (b)	Yes	Y		DL	1	WLZ	.6										
5	IBC 16-12 (a) (c)	Yes	Y		DL	1	WLX	-.6										
6	IBC 16-12 (a) (d)	Yes	Y		DL	1	WLZ	-.6										
7	IBC 16-13 (a) (a)	Yes	Y		DL	1	WLX	.45	LL	.75	LLS	.75						
8	IBC 16-13 (a) (b)	Yes	Y		DL	1	WLZ	.45	LL	.75	LLS	.75						
9	IBC 16-13 (a) (c)	Yes	Y		DL	1	WLX	-.45	LL	.75	LLS	.75						
10	IBC 16-13 (a) (d)	Yes	Y		DL	1	WLZ	-.45	LL	.75	LLS	.75						
11	IBC 16-15 (a)	Yes	Y		DL	.6	WLX	.6										
12	IBC 16-15 (b)	Yes	Y		DL	.6	WLZ	.6										
13	IBC 16-15 (c)	Yes	Y		DL	.6	WLX	-.6										
14	IBC 16-15 (d)	Yes	Y		DL	.6	WLZ	-.6										

Envelope Joint Reactions

	Joint		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N11	max	.523	5	1.632	6	.571	14	0	14	0	14	0	14
2		min	-.41	11	-1.052	12	-.628	4	0	1	0	1	0	1
3	N16	max	.097	13	1.618	4	.184	6	0	14	0	14	0	14
4		min	-.21	3	-1.063	14	-.127	12	0	1	0	1	0	1
5	N18	max	.152	6	.016	4	.263	6	0	14	0	14	0	14
6		min	-.153	4	.009	14	-.264	4	0	1	0	1	0	1
7	N17	max	.101	4	.016	4	.174	14	0	14	0	14	0	14
8		min	-.1	14	.009	14	-.175	4	0	1	0	1	0	1
9	Totals:	max	.646	13	.739	10	1.178	14						
10		min	-.646	3	.443	11	-1.178	4						

Envelope Joint Displacements

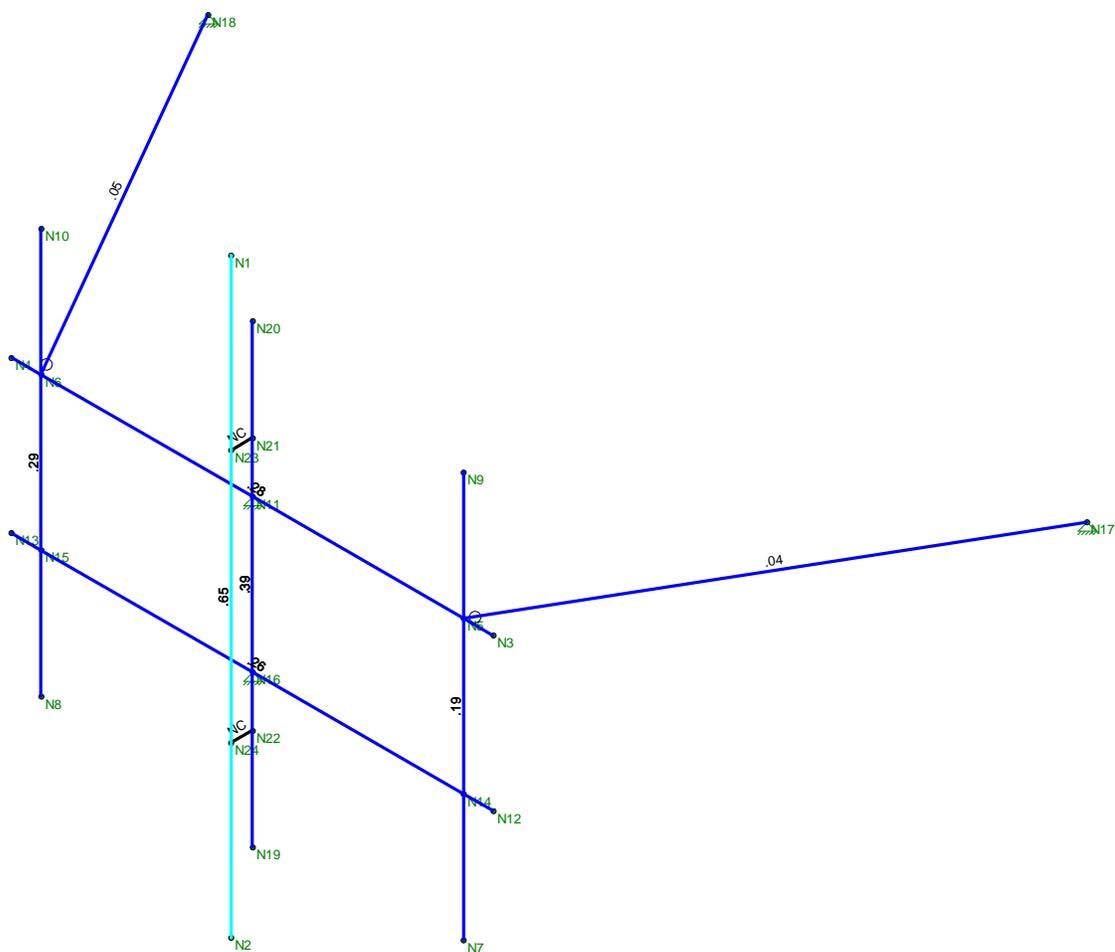
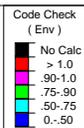
	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotatio...	LC	Z Rotation [rad]	LC
1	N1	max	.287	11	.017	14	.544	4	1.569e-02	4	1.351e-03	11	7.764e-03	5
2		min	-.301	5	-.021	4	-.513	14	-1.504e-02	14	-1.371e-03	5	-7.503e-03	11
3	N2	max	.05	3	.014	14	.111	14	3.032e-03	4	1.533e-03	4	9.868e-04	3
4		min	-.036	13	-.017	4	-.141	4	-2.413e-03	14	-1.509e-03	14	-7.415e-04	13
5	N3	max	0	3	-.027	13	.002	4	2.032e-03	4	2.126e-04	5	-2.208e-04	13
6		min	0	13	-.098	3	-.002	14	-1.917e-03	14	-1.937e-04	11	-9.721e-04	3
7	N4	max	0	14	-.058	11	.008	4	2.494e-03	6	8.003e-04	12	1.212e-03	5
8		min	0	4	-.13	5	-.007	14	-2.393e-03	12	-8.088e-04	6	4.465e-04	11
9	N5	max	0	3	-.025	13	.001	4	2.032e-03	4	2.126e-04	5	-2.202e-04	13
10		min	0	13	-.091	3	-.001	14	-1.917e-03	14	-1.937e-04	11	-9.71e-04	3
11	N6	max	0	14	-.054	11	.002	4	2.494e-03	6	7.99e-04	12	1.211e-03	5
12		min	0	4	-.121	5	-.002	14	-2.393e-03	12	-8.074e-04	6	4.458e-04	11
13	N7	max	-.009	13	-.025	13	.013	13	3.108e-04	3	3.18e-04	6	-3.143e-04	13
14		min	-.027	3	-.091	3	-.021	3	-1.863e-04	13	-2.443e-04	12	-8.754e-04	3
15	N8	max	.058	3	-.055	11	.374	12	6.811e-03	6	3.487e-03	12	2.052e-03	3
16		min	-.007	13	-.122	5	-.379	6	-6.721e-03	12	-3.556e-03	6	-3.998e-04	13
17	N9	max	.047	3	-.025	13	.1	4	3.723e-03	4	2.126e-04	5	5.774e-04	13
18		min	-.011	13	-.092	3	-.096	14	-3.606e-03	14	-1.937e-04	11	-1.771e-03	3
19	N10	max	-.001	11	-.054	11	.033	6	6.893e-04	6	7.99e-04	12	1.76e-03	5
20		min	-.049	5	-.121	5	-.03	12	-5.88e-04	12	-8.074e-04	6	-1.02e-04	11
21	N11	max	0	14	0	14	0	14	2.376e-03	4	5.173e-04	11	1.449e-03	5
22		min	0	1	0	1	0	1	-2.163e-03	14	-5.226e-04	5	-1.092e-03	11
23	N12	max	0	11	-.027	13	.013	14	3.109e-04	3	3.194e-04	6	-2.067e-04	13
24		min	0	5	-.098	3	-.017	4	-1.864e-04	13	-2.457e-04	12	-9.85e-04	3
25	N13	max	0	3	-.061	11	.202	12	5.866e-03	6	3.488e-03	12	1.289e-03	3
26		min	0	13	-.127	5	-.205	6	-5.768e-03	12	-3.557e-03	6	3.703e-04	13
27	N14	max	0	11	-.025	13	.015	14	3.109e-04	3	3.18e-04	6	-2.06e-04	13
28		min	0	5	-.091	3	-.019	4	-1.864e-04	13	-2.443e-04	12	-9.839e-04	3
29	N15	max	0	3	-.054	11	.177	12	5.866e-03	6	3.487e-03	12	1.288e-03	3
30		min	0	13	-.121	5	-.18	6	-5.768e-03	12	-3.556e-03	6	3.696e-04	13
31	N16	max	0	14	0	14	0	14	4.069e-04	6	1.75e-03	4	4.416e-04	3
32		min	0	1	0	1	0	1	-1.799e-04	12	-1.738e-03	14	-8.308e-05	13
33	N17	max	0	14	0	14	0	14	2.319e-03	4	1.098e-03	3	1.124e-03	6
34		min	0	1	0	1	0	1	6.098e-04	14	-1.094e-03	13	-6.863e-04	12
35	N18	max	0	14	0	14	0	14	2.857e-03	6	1.092e-03	11	9.107e-04	14
36		min	0	1	0	1	0	1	7.47e-04	12	-1.097e-03	5	-1.276e-03	4

Envelope Joint Displacements (Continued)

	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotatio...	LC	Z Rotation [rad]	LC
37	N19	max	.027	3	0	14	.076	14	3.29e-03	4	1.533e-03	4	7.86e-04	3
38		min	-.017	13	0	4	-.096	4	-2.67e-03	14	-1.509e-03	14	-5.404e-04	13
39	N20	max	.106	11	0	12	.146	4	4.202e-03	4	1.351e-03	11	3.485e-03	5
40		min	-.115	5	0	6	-.126	14	-3.568e-03	14	-1.371e-03	5	-3.235e-03	11
41	N21	max	.028	11	0	12	.045	4	4.202e-03	4	1.351e-03	11	3.429e-03	5
42		min	-.032	5	0	6	-.04	14	-3.568e-03	14	-1.371e-03	5	-3.179e-03	11
43	N22	max	.008	3	0	14	.012	14	3.291e-03	4	1.533e-03	4	7.306e-04	3
44		min	-.004	13	0	4	-.017	4	-2.67e-03	14	-1.509e-03	14	-4.85e-04	13
45	N23	max	.035	11	.017	14	.045	4	4.202e-03	4	1.351e-03	11	3.429e-03	5
46		min	-.039	5	-.02	4	-.04	14	-3.568e-03	14	-1.371e-03	5	-3.179e-03	11
47	N24	max	.013	3	.014	14	.012	14	3.291e-03	4	1.533e-03	4	7.306e-04	3
48		min	-.009	13	-.017	4	-.017	4	-2.67e-03	14	-1.509e-03	14	-4.85e-04	13

Envelope AISC 14th(360-10): ASD Steel Code Checks

Member	Shape	Code Check	Lo...	LC	She...Lo...	Dir	...Pnc/...	Pnt/o...	Mny...	Mnz...	Cb	Eqn
1	M1	PIPE 2.0	.654	3....	4	.0503....	4	4.808	21.377	1.245	1.245	4.89 H1-...
2	M8	PIPE 2.0	.388	6	14	.120 6	4	8.08	21.377	1.245	1.245	2.5... H1-...
3	M3	PIPE 2.0	.286	5.5	4	.1093.5	6	9.924	21.377	1.245	1.245	4.9... H1-...
4	M2	PIPE 2.0	.283	4.75	3	.1184.75	4	7.252	21.377	1.245	1.245	1.8... H1-...
5	M5	PIPE 2.0	.262	4.75	5	.1394.75	4	7.252	21.377	1.245	1.245	1.8... H1-...
6	M4	PIPE 2.0	.188	5.5	4	.0285.5	3	9.924	21.377	1.245	1.245	4.9... H1-...
7	M6	PIPE 2.0	.047	4....	6	.0048....	5	8.084	21.377	1.245	1.245	1.1... H1-...
8	M7	PIPE 2.0	.042	4....	3	.0048....	5	8.084	21.377	1.245	1.245	1.1... H1-...



Member Code Checks Displayed (Enveloped)
Envelope Only Solution

Centek	CT11328F - Mount Unity Check	
TJL		July 6, 2021 at 11:21 AM
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RADIO FREQUENCY EMISSIONS ANALYSIS REPORT
EVALUATION OF HUMAN EXPOSURE POTENTIAL
TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CT11328F

Marine Sys. Smoke Stack
50 Maple Street
Branford, Connecticut 06405

July 19, 2021

EBI Project Number: 6221003830

Site Compliance Summary	
Compliance Status:	COMPLIANT
Site total MPE% of FCC general population allowable limit:	35.13%

July 19, 2021

T-Mobile

Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, Connecticut 06002

Emissions Analysis for Site: CT11328F - Marine Sys. Smoke Stack

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **50 Maple Street in Branford, Connecticut** for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The number of $\mu\text{W}/\text{cm}^2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately $400 \mu\text{W}/\text{cm}^2$ and $467 \mu\text{W}/\text{cm}^2$, respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 11 GHz frequency bands is $1000 \mu\text{W}/\text{cm}^2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 50 Maple Street in Branford, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top of a 6-foot person standing at the base of the tower. For power density calculations, the broadcast footprint of the AIR6449 antenna has been considered. Due to the beamforming nature of this antenna, the actual beam locations vary depending on demand and are narrow in nature. Using the broadcast footprint accounts for the potential location of beams at any given time.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 LTE channels (600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) 1 NR channel (600 MHz Band) was considered for each sector of the proposed installation. This Channel has a transmit power of 80 Watts.
- 3) 2 LTE channels (700 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 4) 4 GSM channels (PCS Band - 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 5) 2 LTE channels (PCS Band - 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.

- 6) 2 UMTS channels (AWS Band - 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 7) 2 LTE channels (AWS Band – 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 8) 1 LTE Traffic channel (LTE IC and 2C BRS Band - 2500 MHz) was considered for each sector of the proposed installation. This Channel has a transmit power of 60 Watts.
- 9) 1 LTE Broadcast channel (LTE IC and 2C BRS Band - 2500 MHz) was considered for each sector of the proposed installation. This Channel has a transmit power of 20 Watts.
- 10) 1 NR Traffic channel (BRS Band - 2500 MHz) was considered for each sector of the proposed installation. This Channel has a transmit power of 120 Watts.
- 11) 1 NR Broadcast channel (BRS Band - 2500 MHz) was considered for each sector of the proposed installation. This Channel has a transmit power of 40 Watts.
- 12) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 13) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 14) The antennas used in this modeling are the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz / 2500 MHz / 2500 MHz channel(s), the RFS APXVAALL24_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz channel(s), the RFS APX16DWV-16DWV-S-E-A20 for the 1900 MHz / 1900 MHz / 2100 MHz / 2100 MHz channel(s) in Sector A, the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz / 2500 MHz / 2500 MHz channel(s), the RFS APXVAALL24_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz channel(s), the RFS APX16DWV-16DWV-S-E-A20 for the 1900 MHz / 1900 MHz / 2100 MHz / 2100 MHz channel(s) in Sector B, the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz / 2500 MHz / 2500 MHz channel(s), the RFS APXVAALL24_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz channel(s), the RFS

APX16DWV-16DWV-S-E-A20 for the 1900 MHz / 1900 MHz / 2100 MHz / 2100 MHz channel(s) in Sector C. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

- 15) The antenna mounting height centerline of the proposed antennas is 96 feet above ground level (AGL).
- 16) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
- 17) All calculations were done with respect to uncontrolled / general population threshold limits.

T-Mobile Site Inventory and Power Data

Sector:	A	Sector:	B	Sector:	C
Antenna #:	1	Antenna #:	1	Antenna #:	1
Make / Model:	Ericsson AIR 6449	Make / Model:	Ericsson AIR 6449	Make / Model:	Ericsson AIR 6449
Frequency Bands:	2500 MHz / 2500 MHz / 2500 MHz / 2500 MHz	Frequency Bands:	2500 MHz / 2500 MHz / 2500 MHz	Frequency Bands:	2500 MHz / 2500 MHz / 2500 MHz
Gain:	22.65 dBd / 17.3 dBd / 22.65 dBd / 17.3 dBd	Gain:	22.65 dBd / 17.3 dBd / 22.65 dBd / 17.3 dBd	Gain:	22.65 dBd / 17.3 dBd / 22.65 dBd / 17.3 dBd
Height (AGL):	96 feet	Height (AGL):	96 feet	Height (AGL):	96 feet
Channel Count:	4	Channel Count:	4	Channel Count:	4
Total TX Power (W):	240 Watts	Total TX Power (W):	240 Watts	Total TX Power (W):	240 Watts
ERP (W):	36,356.09	ERP (W):	36,356.09	ERP (W):	36,356.09
Antenna A1 MPE %:	16.14%	Antenna B1 MPE %:	16.14%	Antenna C1 MPE %:	16.14%
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	RFS APXVAALL24_43-U-NA20	Make / Model:	RFS APXVAALL24_43-U-NA20	Make / Model:	RFS APXVAALL24_43-U-NA20
Frequency Bands:	600 MHz / 600 MHz / 700 MHz	Frequency Bands:	600 MHz / 600 MHz / 700 MHz	Frequency Bands:	600 MHz / 600 MHz / 700 MHz
Gain:	12.95 dBd / 12.95 dBd / 13.65 dBd	Gain:	12.95 dBd / 12.95 dBd / 13.65 dBd	Gain:	12.95 dBd / 12.95 dBd / 13.65 dBd
Height (AGL):	96 feet	Height (AGL):	96 feet	Height (AGL):	96 feet
Channel Count:	5	Channel Count:	5	Channel Count:	5
Total TX Power (W):	200 Watts	Total TX Power (W):	200 Watts	Total TX Power (W):	200 Watts
ERP (W):	4,151.83	ERP (W):	4,151.83	ERP (W):	4,151.83
Antenna A2 MPE %:	4.39%	Antenna B2 MPE %:	4.39%	Antenna C2 MPE %:	4.39%
Antenna #:	3	Antenna #:	3	Antenna #:	3
Make / Model:	RFS APX16DWW-16DWW-S-E-A20	Make / Model:	RFS APX16DWW-16DWW-S-E-A20	Make / Model:	RFS APX16DWW-16DWW-S-E-A20
Frequency Bands:	1900 MHz / 1900 MHz / 2100 MHz / 2100 MHz	Frequency Bands:	1900 MHz / 1900 MHz / 2100 MHz / 2100 MHz	Frequency Bands:	1900 MHz / 1900 MHz / 2100 MHz / 2100 MHz
Gain:	15.9 dBd / 15.9 dBd / 15.9 dBd / 15.9 dBd	Gain:	15.9 dBd / 15.9 dBd / 15.9 dBd / 15.9 dBd	Gain:	15.9 dBd / 15.9 dBd / 15.9 dBd / 15.9 dBd
Height (AGL):	96 feet	Height (AGL):	96 feet	Height (AGL):	96 feet
Channel Count:	10	Channel Count:	10	Channel Count:	10
Total TX Power (W):	420 Watts	Total TX Power (W):	420 Watts	Total TX Power (W):	420 Watts
ERP (W):	16,339.90	ERP (W):	16,339.90	ERP (W):	16,339.90
Antenna A3 MPE %:	7.25%	Antenna B3 MPE %:	7.25%	Antenna C3 MPE %:	7.25%

Site Composite MPE %	
Carrier	MPE %
T-Mobile (Max at Sector A):	27.77%
Sprint	7.36%
Site Total MPE % :	35.13%

T-Mobile MPE % Per Sector	
T-Mobile Sector A Total:	27.77%
T-Mobile Sector B Total:	27.77%
T-Mobile Sector C Total:	27.77%
Site Total MPE % :	35.13%

T-Mobile Maximum MPE Power Values (Sector A)							
T-Mobile Frequency Band / Technology (Sector A)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ($\mu\text{W}/\text{cm}^2$)	Frequency (MHz)	Allowable MPE ($\mu\text{W}/\text{cm}^2$)	Calculated % MPE
T-Mobile 2500 MHz LTE IC & 2C Traffic	1	11044.63	96.0	49.02	2500 MHz LTE IC & 2C Traffic	1000	4.90%
T-Mobile 2500 MHz LTE IC & 2C Broadcast	1	1074.06	96.0	4.77	2500 MHz LTE IC & 2C Broadcast	1000	0.48%
T-Mobile 2500 MHz NR Traffic	1	22089.26	96.0	98.04	2500 MHz NR Traffic	1000	9.80%
T-Mobile 2500 MHz NR Broadcast	1	2148.13	96.0	9.53	2500 MHz NR Broadcast	1000	0.95%
T-Mobile 600 MHz LTE	2	591.73	96.0	5.25	600 MHz LTE	400	1.31%
T-Mobile 600 MHz NR	1	1577.94	96.0	7.00	600 MHz NR	400	1.75%
T-Mobile 700 MHz LTE	2	695.22	96.0	6.17	700 MHz LTE	467	1.32%
T-Mobile 1900 MHz GSM	4	1167.14	96.0	20.72	1900 MHz GSM	1000	2.07%
T-Mobile 1900 MHz LTE	2	2334.27	96.0	20.72	1900 MHz LTE	1000	2.07%
T-Mobile 2100 MHz UMTS	2	1167.14	96.0	10.36	2100 MHz UMTS	1000	1.04%
T-Mobile 2100 MHz LTE	2	2334.27	96.0	20.72	2100 MHz LTE	1000	2.07%
						Total:	27.77%

• NOTE: Totals may vary by approximately 0.01% due to summation of remainders in calculations.

Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

T-Mobile Sector	Power Density Value (%)
Sector A:	27.77%
Sector B:	27.77%
Sector C:	27.77%
T-Mobile Maximum MPE % (Sector A):	27.77%
Site Total:	35.13%
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **35.13%** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.